

# Multiphase Polarization in Ion-Intercalation Nanofilms: General Theory Including Various Surface Effects and Memory Applications

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Ion concentration polarization (CP, current-induced concentration gradient adjacent to a charge-selective interface) has been well studied for single-phase mixed conductors (e.g., liquid electrolyte), but multiphase CP has been rarely addressed in literature. In our recent publication, we proposed that CP above certain threshold currents can flip the phase distribution in multiphase ion-intercalation nanofilms sandwiched by ion-blocking electrodes. This phenomenon is known as multiphase polarization (MP). It is then proposed that MP can further lead to nonvolatile interfacial resistive switching (RS) for asymmetric electrodes with ion-modulated electron transfer, which theory can reproduce the experimental results of LTO memristors. In this study, a comprehensive 2D phase-field model is derived for coupled ion-electron transport in ion-intercalation materials, with surface effects including electron transfer kinetics, non-neutral wetting, energy relaxation, and surface charge. Then, the model is used to study MP. Time evolution of phase boundaries is presented, and analyze the switching time, current, energy, and cyclic voltammetry, for various boundary conditions. It is found that the switching performance can be improved significantly by manipulating surface conditions and mean concentration. Finally, the prospects of MP-based memories and possible extensions of the current model is discussed.

## 1. Introduction

Ion-intercalation materials, which allow reversible insertion of host ions (along with electrons) and ion-modulation of certain physical properties (e.g., thermodynamic, electronic, optical, and magnetic properties), play important roles in various applications such as energy storage,<sup>[1]</sup> ion separation,<sup>[2,3]</sup> electrochromic display,<sup>[4]</sup> and very recently, information storage and computing.<sup>[5,6]</sup> Many commonly used ion-intercalation materials<sup>[1]</sup> (e.g.,  $\text{Li}_{4+3x}\text{Ti}_5\text{O}_{12}$  (LTO),<sup>[7]</sup>  $\text{Li}_x\text{FePO}_4$  (LFP)<sup>[8]</sup>) exhibit multiphase behaviours and mixed ion-electron conductivity. Therefore, it is important to understand the coupled ion-electron transport within and at the interfaces of multiphase ion-intercalation materials, especially at high electric currents during rapid operations,<sup>[6,9]</sup> but related studies are still limited.

The multiphase ion-intercalation materials can spontaneously split into ion-rich and ion-poor phases if the mean ion concentration falls in the spinodal region,

where co-existing phases are thermodynamically more stable than single phase.<sup>[10]</sup> Numerous phase-field models have been developed to study the multiphase ion intercalation processes and have brought lots of insights to applications such as Li-ion batteries.<sup>[8,11–14]</sup> However, most phase-field models do not consider coupled ion-electron transport.<sup>[8,11–14]</sup> They first solve the transport of neutral ion-electron pairs during intercalation, which is a pure diffusion problem with a flux boundary (Cahn–Hilliard reaction model<sup>[12]</sup>) or a diffusion-reaction problem without boundary flux (Allen–Cahn model<sup>[12]</sup>). And then they calculate the ion-modulated electronic conductance if needed.<sup>[15,16]</sup> This simplification works well if the electronic conductivity is much larger than ionic conductivity and the applied current is not too large, regardless of the multiphase behaviors.<sup>[17,18]</sup> Otherwise, the coupling of ion and electron transport may not be neglected.

Much research has been done for the coupling of ion and electron transport within and at interfaces of single-phase ion-electron conductors.<sup>[17–20]</sup> For example, it is known that high electronic currents can lead to ion concentration polarization (CP, ion enrichment on one electrode and depletion on the other) in a mixed ion-electron conductor between

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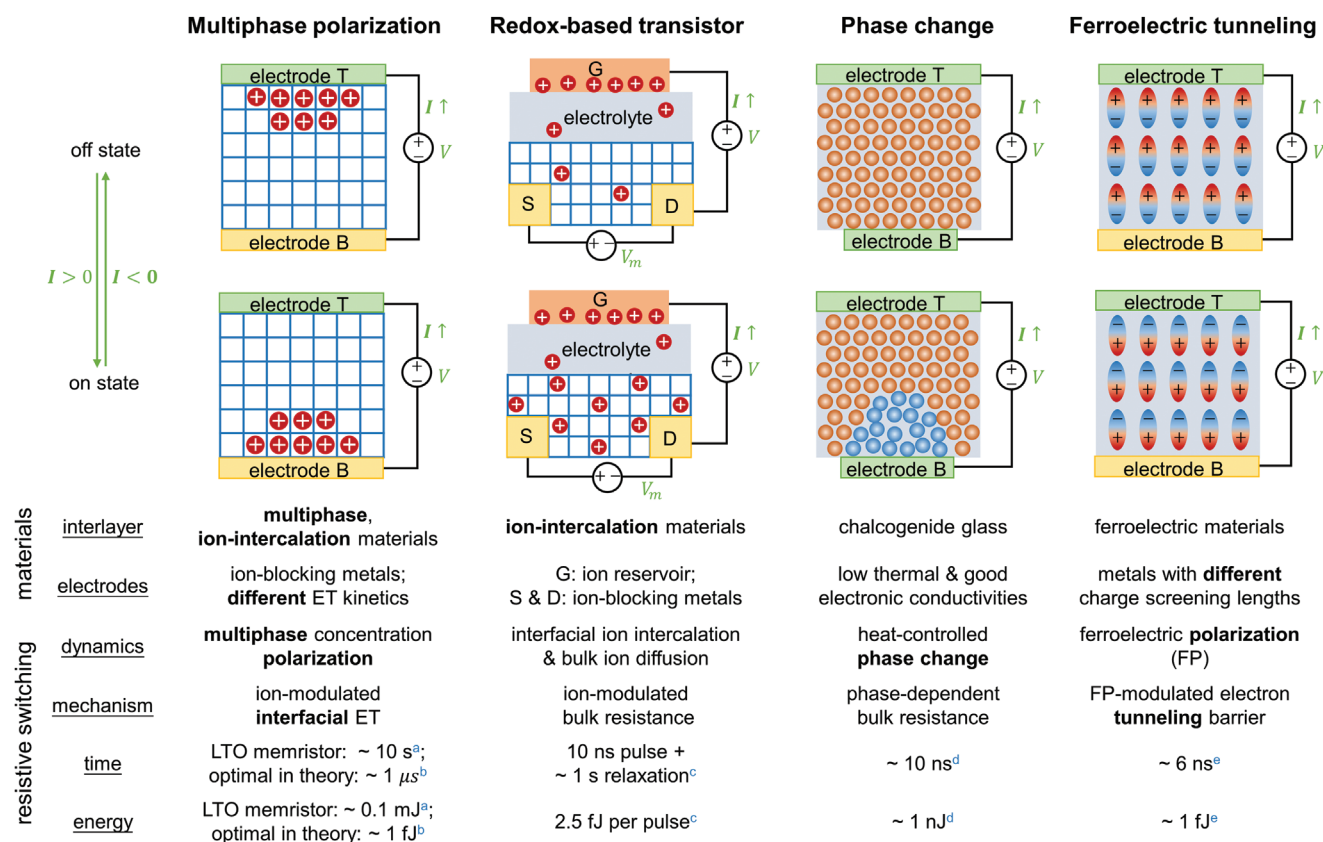
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DOI: 10.1002/adfm.202213621



**Figure 1.** Comparison between four nonvolatile resistive switching mechanisms: multiphase polarization (MP, this work), redox-based transistor (RBT), phase change (PC), and ferroelectric tunneling (FT). ET represents for electron transfer. Only single crystals are drawn for simplicity, but polycrystals are common in real devices. References: a, estimated from Figure 2c in Ref. [5] (see the calculation in Section 5.2.2); b, prediction in this work (Section 6); c, Ref. [6]; d, Ref. [27]; e, Ref. [28].

ion-blocking electrodes. This CP can influence the measurement of electronic conductivity,<sup>[21]</sup> and lead to some volatile memristive behaviors of semiconductors.<sup>[22]</sup> CP has also been well studied in liquid electrolytes and has been utilized for water treatment.<sup>[23–25]</sup> However, coupled ion-electron transport such as CP for multiphase ion-intercalation materials remain poorly addressed in the literature.

In our recent work,<sup>[26]</sup> we described the CP in multiphase ion-intercalation materials between ion-blocking electrodes, based on a 1D preliminary phase-field model for coupled cation-electron transport. At high electric currents, multiphase CP can lead to phase redistribution, a phenomenon we call multiphase polarization (MP). As shown in the first panel of **Figure 1**, a large enough downward electric current in the nanofilm can drive the ion-rich phase to the bottom electrode or drive the ion-poor phase to the top electrode, and an upward current can drive the opposite process. Unlike CP which disappears at zero currents, MP is nonvolatile since the altered phase distribution remains even after removal of the currents. We then assumed that interfacial electron transfer resistance dominates the total resistance and strongly depends on local ion concentration, therefore MP-induced interfacial phase change (IPC) can lead to non-volatile interfacial resistive switching (RS) if the two electrodes are asymmetric. We then gave a thorough analysis of the switching time and current, resistance ratio, and cyclic

voltammetry behaviors for the MP mechanism using a 1D preliminary model with natural boundary condition (zero normal gradient of concentration), and qualitatively reproduced the experimental RS behaviors of LTO memristors (made from LTO nanofilm sandwiched by Pt electrodes).<sup>[5]</sup> Note that MP itself is a more general concept, while MP-based RS has more requirements for the ion-intercalation materials and electrodes (more discussion can be found in Section 6).

Nowadays, conventional computing architectures are facing the problems of von Neumann bottleneck (limited data transfer between CPU and memory) along with data explosion, as well as the end of Moores' Law due to the increasing cost for down-scaling.<sup>[29]</sup> The above problems can be solved by in-memory computing, which can be realized using high-performance non-volatile RS devices.<sup>[29,30]</sup> Such devices can have two-terminal or three-terminal structures, and two-terminal ones are usually also called memristors. We can then compare MP with other well-known and relevant non-volatile RS mechanisms,<sup>[29,30]</sup> including redox reactions,<sup>[31–35]</sup> phase change,<sup>[27,35–37]</sup> and ferroelectric tunneling,<sup>[38–41]</sup> as shown in Figure 1. Redox-based mechanisms usually change the bulk resistance of a nanofilm by injecting charge carriers through an active electrode.<sup>[29–35]</sup> Many redox-based memristors involves the formation of conductive filaments.<sup>[29,30]</sup> Recently, great progress has been made in filament-free redox-based transistors (RBT) using ion-intercalation

materials with ion-modulated conductivity.<sup>[6,42–44]</sup> Compared with RBT, MP has conserved total amount of ions during switching and mainly changes surface resistance instead of bulk resistance. The so-called phase change (PC) mechanism usually uses Joule heating to switch between amorphous and crystalline phases which have different bulk resistance,<sup>[27,29,30,36]</sup> while MP uses electric field to move ion-modulated phases which can change interfacial resistance. In the ferroelectric tunneling (FT) mechanism, the ferroelectric polarization switchable by a threshold voltage can change the tunneling current if the two electrodes have different charge screening length.<sup>[29,30,40,41]</sup> Interestingly, MP and FT are in some sense conceptually similar, since both of them utilize some non-volatile polarization of the bulk materials and the asymmetry of the electrodes to change the total resistance. In Section 6, we will make more comparison about the performance of these mechanisms.

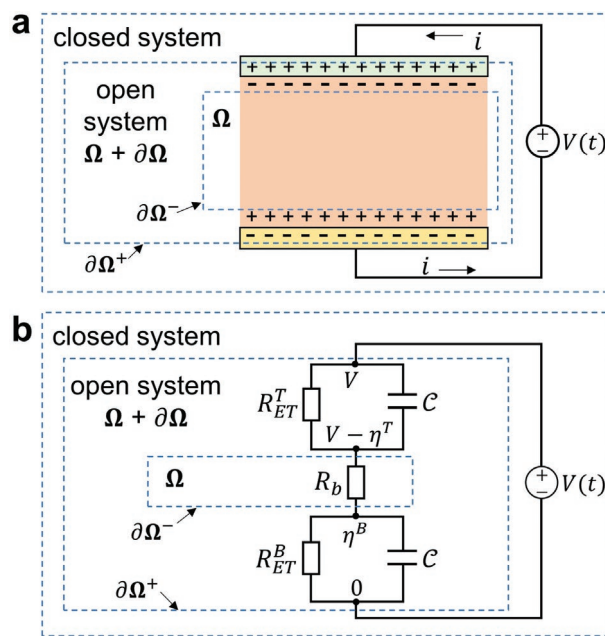
In this work, we aim to develop a comprehensive and general phase field model for coupled, multiphase ion-electron transport with electron transfer kinetics, non-neutral wetting, energy relaxation and electric double layer at the electrode-nanofilm interfaces. To the best of our knowledge, this model is the first non-equilibrium model to consider surface energy relaxation and surface charge of multiphase ion-intercalation materials. Then we use the new model to analyze 2D MP with various surface effects included, and present discussion in the general outlook.

The paper is organized as below. We first present the derivation of the phase-field model in Section 2, and then do some thermodynamic and kinetic analysis of the model in Section 3. In Section 4, we apply the general model to regular solutions to model ion-intercalation material, and list all the dimensionless equations to be solved. We then simulate 2D MP at various conditions, and compare the results with the old 1D model in Section 5. Finally, we discuss the prospects of MP-based memristors and the model itself, and give a conclusion in Section 6.

## 2. General Phase-Field Model

### 2.1. Introduction

In this section, we derive a general phase-field model for multiphase coupled ion-electron transport in a nanofilm with thickness  $L$  sandwiched between two parallel ion-blocking electrodes, as shown in Figure 2a. We expect that a voltage applied to the electrodes can result in electron transfer and charge accumulation at the electrode-nanofilm interfaces, as well as phase re-distribution in the nanofilm. Following our previous work,<sup>[26]</sup> we consider three species in the mixed ion-electron conductor: monovalent cations “p”, electrons “n”, and immobile positively charged defects “d”. We assume that the mobile cations and electrons are fully dissociated and ignore the generation and combination of charge carriers. We also assume constant pressure and temperature, and ignore mechanical effects and volume change (a good assumption for “zero strain” materials like  $\text{Li}_{4+3x}\text{Ti}_5\text{O}_{12}$ <sup>[7]</sup> and  $\text{Li}_x\text{WO}_3$ <sup>[45]</sup>). In addition, we assume that the total resistance is dominated by surface resistance thus the potential drop in the bulk (usually within several thermal voltages in each phase) is very small compared with the total potential drop (up to hundreds of thermal voltages). Furthermore, we



**Figure 2.** a) The model system that we consider in this work and b) its equivalent circuit model when the interlayer is homogeneous.

consider large ion concentration (thousands of moles per cubic meter, which is typical for ion-intercalation materials) so that the space charge should be very thin compared with the nanofilm (10–100 nm).

Then we can divide the open system shown in Figure 2a into two parts: the bulk domain  $\Omega$ , and the surface  $\partial\Omega$ . We assume no electrostatic energy everywhere in  $\Omega$  (which can lead to local electroneutrality), and put the electric double layer (EDL, formed by charge from the nanofilm and the electrode) with net neutrality into  $\partial\Omega$ . We ignore the diffuse part of EDL since we consider large ion concentration. In addition, we ignore the EDL at phase boundaries (interfaces between different phases), whose contribution to phase boundary energy (and potential drop) should not change much with currents due to the assumed small bulk resistance. In another word, we can just control the effective phase boundary energy by adjusting some parameters (e.g.,  $\kappa_p$  in Section 3.3) without modeling the EDL explicitly at phase boundaries. The above treatment greatly simplifies the problem and can provide lots of insights. Then the total Gibbs free energy of the open system can be expressed as:

$$G(c_p, c_n, \phi) = G_b + G_s = \int_{\Omega} g dV + \int_{\partial\Omega} \gamma_s dS \quad (1)$$

where  $c_p$  and  $c_n$  are the molar concentration of the cations and the electrons,  $\phi$  is the electric potential,  $g$  is the local free energy density in the bulk  $\Omega$ , and  $\gamma_s$  is the surface energy density on  $\partial\Omega$ .

Next, based on the first and second laws of thermodynamics, the total Gibbs free energy  $\mathcal{G}$  of the closed system in Figure 2 at constant pressure and temperature should not increase with time.<sup>[46]</sup> If we assume no energy dissipation in the voltage source, we have

$$\frac{\partial \mathcal{G}}{\partial t} = \frac{\partial G}{\partial t} + \int_{\partial\Omega} + \mu_n \mathbf{J}_n \cdot \mathbf{n} dS \leq 0 \quad (2)$$

where the integral is the energy flux out of the open system (or the energy flux into the voltage source),  $\mu_n$  is the electrochemical potential of electrons,  $\mathbf{J}_n$  is the flux of electrons, and  $\mathbf{n}$  is the normal vector on  $\partial\Omega$  to point outward of  $\Omega$ . Noting that the energy flux into and out  $\partial\Omega$  may not be the same, we denote  $\partial\Omega^+$  and  $\partial\Omega^-$  as the outer (electrode) and inner (nanofilm) side of  $\partial\Omega$ , respectively. For the convenience of mathematical derivation, we can further split  $\frac{\partial\mathcal{G}}{\partial t}$  into two parts  $\frac{\partial\mathcal{G}}{\partial t} = \frac{\partial\mathcal{G}_1}{\partial t} + \frac{\partial\mathcal{G}_2}{\partial t}$ :

$$\frac{\partial\mathcal{G}_1}{\partial t} = \frac{\partial G_b}{\partial t} + \int_{\partial\Omega} \mu_n \mathbf{J}_n \cdot \mathbf{n} dS \quad (3)$$

$$\frac{\partial\mathcal{G}_2}{\partial t} = \frac{\partial G_s}{\partial t} + \int_{\partial\Omega^+} \mu_n \mathbf{J}_n \cdot \mathbf{n} dS - \int_{\partial\Omega^-} \mu_n \mathbf{J}_n \cdot \mathbf{n} dS \quad (4)$$

In the following of this section, we derive  $\frac{\partial\mathcal{G}_1}{\partial t}$  and the corresponding bulk equations in Section 2.2, derive  $\frac{\partial\mathcal{G}_2}{\partial t}$  and the corresponding boundary conditions in Section 2.3, and give a summary and discussion in Section 2.4.

## 2.2. Bulk Energy Evolution

In this part, we derive  $\frac{\partial\mathcal{G}_1}{\partial t}$  and the corresponding bulk governing equations. In  $\Omega$ , we assume the local free energy density  $g$  is just the summation of the free energy density for each species

$$g = g_p + g_n + g_d \quad (5)$$

We then assume the fixed charge “d” only has electrostatic energy,

$$g_d = z_d c_d F \phi \quad (6)$$

and the mobile species “p”, “n” have chemical energy, electrostatic energy, and Cahn-Hilliard gradient energy<sup>[12,19,47,48]</sup>:

$$g_k(c_k, \phi) = g_{k,chem}(c_k) + z_k c_k F \phi + \frac{1}{2} \kappa_k |\nabla c_k|^2 \quad (7)$$

where  $z_k$  is the valence of species  $k$ ,  $F$  is the Faraday constant,  $\phi$  is the electric potential, and  $\kappa_k$  is the diagonal gradient energy coefficient (assumed to be a constant). In this work, we further assume  $\kappa_n = 0$ , which can help us simplify the expression for surface energy in Section 2.3. Note that here we have neglected the electrostatic energy term  $-\frac{1}{2} \epsilon |\nabla\phi|^2$  in  $g$  ( $\epsilon$  is the permittivity), which can lead to space charge<sup>[19,48]</sup> and dielectric breakdown (if  $\epsilon$  is a nonlinear function of ion concentration)<sup>[15,49,50]</sup> at high electric fields. This treatment is reasonable in this work, since we have assumed small bulk electric fields (within a few thermal voltages over 100 nm) and thin space charge (due to the assumed large concentration), and have put space charge into  $\partial\Omega$ . In addition, since we ignore the generation-recombination of electrons and ions, the conservation of species leads to

$$\frac{\partial c_k}{\partial t} + \nabla \cdot \mathbf{J}_k = 0 \quad (8)$$

where  $\mathbf{J}_k$  is the flux of species  $k$ .

Now after some algebra (see Appendix A), we get

$$\begin{aligned} \frac{\partial\mathcal{G}_1}{\partial t} &= \sum_{k=p,n} \int_{\Omega} \nabla \mu_k \cdot \mathbf{J}_k dV \\ &+ \int_{\Omega} \left( \sum_{k=p,n,d} z_k c_k F \right) \frac{\partial\phi}{\partial t} dV \\ &+ \int_{\partial\Omega} \kappa_p \mathbf{n} \cdot \nabla c_p \frac{\partial c_p}{\partial t} dS \end{aligned} \quad (9)$$

where  $\mu_k$  is the electrochemical potential of species  $k$  in the nanofilm<sup>[12]</sup>

$$\begin{aligned} \mu_k &= \frac{\partial g_k}{\partial c_k} - \nabla \cdot \frac{\partial g_k}{\partial \nabla c_k} \\ &= \mu_{k,chem} + z_k F \phi - \kappa_k \nabla^2 c_k \end{aligned} \quad (10)$$

where  $\mu_{k,chem} = \frac{\partial g_{k,chem}}{\partial c_k}$  is the chemical potential. The surface integral in Equation (9) can be combined with  $\frac{\partial\mathcal{G}_2}{\partial t}$  to get the boundary conditions in Section 2.3. Now we can get the bulk governing equations that ensures the volume integrals in Equation (9) minimize spontaneously

$$\mathbf{J}_k = -\frac{D_k c_k}{RT} \nabla \mu_k \quad (11)$$

$$c = c_p = -(z_n c_n + z_d c_d) / z_p \quad (12)$$

where  $D_k$  is the diffusivity,  $R$  is the gas constant. The corresponding conductivity is  $\sigma_k = D_k F^2 z_k^2 c_k / RT$ . Equation (11) assumes that the flux is linear with the gradient of  $\mu_k$  which should work well for near-equilibrium dynamics. Equation (12) is the electroneutrality equation, which reduces the two variables  $c_p$  and  $c_n$  into one variable  $c$ . Taking  $z_p = 1$ ,  $z_n = -1$ ,  $z_d = 1$ , we can reduce Equation (12) to

$$c = c_p = c_n - c_d \quad (13)$$

## 2.3. Surface Energy Evolution

Next we derive  $\frac{\partial\mathcal{G}_2}{\partial t}$  and get the boundary conditions. We first need to zoom in to see the internal structure of the surface. Inside  $\partial\Omega$ , we assume there is a net-neutral EDL composed of parallel, infinitely-thin, and opposite charges that are separated by a small distance  $d_s$  and formed by excess/lack of electrons on the surfaces of the nanofilm and electrode, respectively. This indicates that the diffuse part and the ionic component of the nanofilm surface charge are both neglected. In the following, we use  $\Delta(\cdot)$  to represent the jump of a surface variable across  $\partial\Omega$  (the variable on the electrode surface minus that on the nanofilm surface). Then we can model the EDL as a linear capacitor with  $\Delta\phi$ -independent capacitance density  $C = \epsilon_s / d_s$  ( $\epsilon_s$  is the permittivity between the two charged surfaces), and get

$$\Gamma = C \Delta\phi \quad (14)$$

where  $\Gamma$  is the surface charge density on the electrode side of the EDL. This linear capacitor without ionic charge greatly simplifies the problem. More complex surface charge models can be considered in future works (see discussion in Section 6). We can further split  $\Delta\phi$  into two parts by defining the overpotential  $\eta$

$$\eta = \frac{1}{z_n F} \Delta\mu_n = \Delta\phi - (\Delta\phi)_0 \quad (15)$$

where  $(\Delta\phi)_0$  is only determined by chemical part of  $\Delta\mu_n$  and thus only depends on  $c$  but not  $\eta$ .

Then we want to derive an expression for surface energy density  $\gamma_s$ , which should only be a function of overpotential  $\eta$  and nearby  $c$  on  $\partial\Omega^-$  (remember that the bulk electroneutrality condition, Equation (13), has reduced  $c_p$  and  $c_n$  to a single parameter  $c$ ). Here we present two approaches.

In the first approach, we notice three contributions of  $\gamma_s$ : the free energy of the surface charges, the electrostatic energy between the surface charges, and the structural energy (non-electric part of the surface energy that may depend on  $c$ ). Since we have assumed  $\kappa_n = 0$ ,  $\Delta\mu_n$  and  $\gamma_s$  should not depend on  $\nabla c$ . Therefore, we have

$$\gamma_s(c, \eta) = \Delta\mu_n \frac{\Gamma}{z_n F} - \frac{1}{2} \epsilon_s \left( \frac{\Delta\phi}{d_s} \right)^2 d_s + \gamma_s^*(c) \quad (16)$$

where we have assumed constant electric field between surface charges, and  $\Gamma$ -independent chemical potential of electrons at the charged surfaces. Then we can substitute Equation (15) into Equation (16), and rearrange Equation (16) to get

$$\gamma_s(c, \eta) = \frac{1}{2} C \eta^2 + \gamma_s^0(c) \quad (17)$$

where  $\gamma_s^0$  is the surface energy density at zero overpotential. Note that  $\gamma_s^*$  does not equal  $\gamma_s^0$  unless  $(\Delta\phi)_0 = 0$ .

In the second approach, we integrate the work done to charge the surfaces as the surface potential drop increases from  $(\Delta\phi)_0$  to  $\Delta\phi$ <sup>[51]</sup>

$$\gamma_s(c, \eta) - \gamma_s^0(c) = \int_{C(\Delta\phi)_0}^{C\Delta\phi} \Delta\mu_n \frac{d\Gamma}{z_n F} = \frac{1}{2} C \eta^2 \quad (18)$$

As we can see, we get the same results from the two approaches. The excess surface energy  $\gamma_s - \gamma_s^0$  is the same as the energy stored in a capacitor at potential drop  $\eta$ . More details for discussion of the signs of the surface energy can be found in Appendix B.

Now we can put  $\gamma_s$  into Equation 4) and get

$$\frac{\partial \mathcal{G}_2}{\partial t} = \int_{\partial\Omega} \frac{\partial \gamma_s^{\text{eff}}}{\partial c} \frac{\partial c}{\partial t} dS - \int_{\partial\Omega} F \eta \mathbf{J}_n^{\text{ET}} \cdot \mathbf{n} dS \quad (19a)$$

$$\frac{\partial \gamma_s^{\text{eff}}}{\partial c} = \frac{\partial \gamma_s^0}{\partial c} - C \eta \frac{\partial (\Delta\phi)_0}{\partial c} + \left( \frac{1}{2} \eta^2 - \eta \Delta\phi \right) \frac{\partial C}{\partial c} \quad (19b)$$

Here we have used  $(\mathbf{J}_n \cdot \mathbf{n})_{\partial\Omega^+} = \mathbf{J}_n^{\text{ET}} \cdot \mathbf{n} + \frac{1}{F} \frac{\partial C \Delta\phi}{\partial t}$  from mass balance for surface charge, where  $\mathbf{J}_n^{\text{ET}} \cdot \mathbf{n}$  is the electron transfer rate between the two charged surfaces as a function of  $c$  and  $\eta$ .  $\gamma_s^{\text{eff}}$  has included energy change of the voltage source compared with  $\gamma_s$ . In addition, if we assume the chemical potential of electrons in electrodes is a constant, then we can plug  $\frac{\partial (\Delta\phi)_0}{\partial c} = \frac{1}{z_n F} \frac{\partial \mu_{n, \text{chem}}}{\partial c}$  into Equation 19b to make it more explicit. In the following, for simplicity, we also assume  $C$  does not depend on  $c$ , though this dependence can be easily added in future works.

Finally, we add  $\frac{\partial \mathcal{G}_1}{\partial t}$  and  $\frac{\partial \mathcal{G}_2}{\partial t}$  together, and let the surface integrals also not increase with time. This can be satisfied by applying the following conditions

$$\frac{\partial \gamma_s^{\text{eff}}}{\partial c} + \kappa_p \nabla c \cdot \mathbf{n} = -\tau_\gamma \frac{\partial c}{\partial t} \quad (20)$$

$$\mathbf{n} \cdot \mathbf{J}_n^{\text{ET}} \eta > 0 \quad (21)$$

In Equation (20),  $\tau_\gamma$  (a positive number) adds relaxation to surface energy and can lead to dynamic contact angle,<sup>[52–55]</sup> and  $\frac{\partial \gamma_s^{\text{eff}}}{\partial c}$  instead of  $\frac{\partial \gamma_s}{\partial c}$  determines steady state surface energy balance (as well as contact angle). We discuss on Equation (20) in detail in Section 3.4. Equation (21) simply requires that the electrons should transfer against the overpotential, which is consistent with the existing electron transfer models like Butler-Volmer equation,<sup>[12,26]</sup> Marcus theory,<sup>[56]</sup> and Schottky diode.<sup>[57]</sup>

## 2.4. Summary and Discussion

Based on Section 2.2 and Section 2.3, now we can write the time evolution of the total free energy of the closed system as

$$\begin{aligned} \frac{\partial \mathcal{G}}{\partial t} &= \int_{\Omega_{k=p,n}} \nabla \mu_k \cdot \mathbf{J}_k dV \\ &+ \int_{\partial\Omega} \left( \frac{\partial \gamma_s^{\text{eff}}}{\partial c} + \kappa_p \nabla c \cdot \mathbf{n} \right) \frac{\partial c}{\partial t} \\ &- \int_{\partial\Omega} \eta F \mathbf{J}_n^{\text{ET}} \cdot \mathbf{n} dS \end{aligned} \quad (22)$$

where the three integrals represent the energy dissipation by bulk transport, surface friction, and interfacial electron transfer, respectively. The energy transfer between the voltage source and surface charges does not change the total free energy.

If we assume homogeneous single phase in the nanofilm, we can analogize the whole system as an electric circuit shown in Figure 2b. In this case, the second integral in Equation (22) disappears. The integrand in the first volume integral becomes

$$\sum_{k=p,n} \nabla \mu_k \cdot \mathbf{J}_k \rightarrow -\sigma |\nabla \phi|^2 \quad (23)$$

where  $\sigma = \sum_{k=p,n} \sigma_k = \sum_{k=p,n} z_k^2 F^2 c_k D_k / RT$  is the bulk conductivity. Therefore, the first integral in Equation (22) represents the energy dissipation on a bulk resistance  $R_b$ . Similarly, the last integral in Equation (22) represents the energy dissipation on two surface resistances  $R_{ET}^T$  and  $R_{ET}^B$  (T: top electrode, B: bottom electrode). In addition, the energy can be transferred between the voltage source and the two surface charge capacitors at electrode-nanofilm interfaces. Each capacitor has capacitance  $C = CA$  ( $A$  is surface area) and potential drop  $\eta$ . Finally, the RC circuit is connected to a voltage source  $V(t)$  to close the system. We can see clearly that in the circuit, the energy input from the voltage source has two destinations: dissipated in the resistances  $R_b$ ,  $R_{ET}^T$  and  $R_{ET}^B$ , or stored in the capacitors.

In this work, we care more about the multiphase behaviours in the nanofilm. In this case, the system is more complex than the circuit model shown in Figure 2b. We assume ion concentration can significantly influence the electron transfer rate at electrode-nanofilm interfaces. Therefore, MP-induced IPC at high electric currents can change the resistance  $R_{ET}^T$  and  $R_{ET}^B$ , leading to RS behaviors.

### 3. Thermodynamic and Kinetic Analysis

In this section, we derive some analytical expressions based on the phase field model, including the phase equilibrium properties, the critical current for MP (switching current), and the surface energy and contact angle. Finally, we compare the surface charge effects in our system with the well-known electrowetting phenomenon.

#### 3.1. Phase Equilibrium

In this part, we analyze the equilibrium state (no flux everywhere) and derive the binodal points, spinodal points, and equilibrium contact angle. To begin with, we define  $g_h$  as the homogeneous part of the total free energy density  $g$ , and define  $\mu_h$  as the homogeneous part of the chemical potential of the neutral ion-electron pairs, respectively

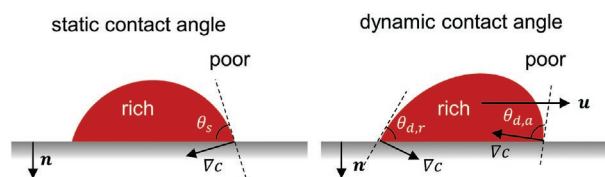
$$g_h = g_{p,chem} + g_{n,chem}, \mu_h = \frac{\partial g_h}{\partial c} \quad (24)$$

Both  $g_h$  and  $\mu_h$  are independent on  $\phi$ , since the total electrostatic energy of species “p”, “n”, “d” is zero due to the assumed bulk electroneutrality.  $\mu_h$  is also called “diffusional chemical potential” of the homogeneous mixture,<sup>[10]</sup> defined as the change in free energy upon adding a neutral ion-electron pair at constant temperature and pressure.

Now we consider a lumped form of Equation (1) at equilibrium state. We assume the concentration inside each phase is uniform, and treat the phase boundary as infinitely thin interface with energy  $\gamma_i$ . We denote the two phases as  $r$  and  $p$  and assume  $c_r > c_p$ . As before, we use  $s$  to denote the walls as a third phase. Then for a 2D system, we have

$$G_{lumped} = g_h(c^r)S^r + g_h(c^p)[S - S^r] + \gamma_i A^{r,p} + [\gamma_s^0(c^r) - \gamma_s^0(c^p)]A^{s,r} + \lambda [c^r S^r + c^p [S - S^r] - c_m S] + const \quad (25)$$

where  $A^{r,p}$  is the contact length between the rich and poor phases,  $A^{r,p}$  is the contact length between the rich phase and the solid wall,  $S$  is the total area and  $S^r$  is the area of the rich phase,  $c_m$  is the mean ion concentration in the nanofilm, and  $\lambda$  is the Lagrange multiplier for species conservation. We then further consider the phase distribution as a rich phase spherical drop sitting on an electrode and surrounded by the poor phase (shown in Figure 3), and get  $A^{r,p} = 2r\theta$ ,  $A^{s,r} = 2r \sin \theta$ ,  $S^r = r^2\theta - r^2 \sin \theta \cos \theta$ , where the curvature radius  $r$  and contact angle  $\theta$  are both defined in the rich phase. Therefore, now  $G_{lumped}$  is a function of five variables:  $c^r$ ,  $c^p$ ,  $\lambda$ ,  $r$ ,  $\theta$ .



**Figure 3.** Schematic for the static and dynamic contact angle, where the contact angle is defined from  $\cos \theta = n \cdot \nabla c / |\nabla c|$ .

Next, by minimizing  $G_{lumped}$  (let first derivatives equal zero), we get the following relation for the binodal points  $c_{b0}$  and  $c_{b1}$  (assume  $c_{b0} < c_{b1}$ )

$$\mu_h(c_{b0}) = \mu_h(c_{b1}) = \frac{g_{b1} - g_{b0} + \frac{\gamma_i}{r_0}}{c_{b1} - c_{b0}} = \mu_b \quad (26)$$

and the Young-Laplace equation

$$\gamma_s^0(c_{b1}) - \gamma_s^0(c_{b0}) = -\gamma_i \cos \theta_s^0 \quad (27)$$

where  $\theta_s^0$  is the equilibrium contact angle defined in the rich phase and  $r_0$  is the equilibrium curvature of the rich phase.

Here we have used  $\frac{\partial \gamma_s^0}{\partial c} |_{c_{b0}, c_{b1}} = 0$ , which is justified in Equation (31) and Equation (36). These two equations are also true for a system of a poor-phase droplet surrounded by rich phase, but note that in this case  $r_0$  is negative. The effect of the curvature of the rich phase on binodal points (term  $\frac{\gamma_i}{r_0}$  in Equation (26)) is essentially analogous to the effect of the curvature of a liquid droplet on the vapor pressure (Kelvin equation or Ostwald–Freundlich equation at constant temperature,<sup>[58–60]</sup> and Gibbs–Thomson equation at constant pressure<sup>[61]</sup>). For the simulations in this paper, we can find that the contribution of surface energy and interface curvature to phase diagram are small (Section 5.1). In this case, we can drop the surface energy related terms in Equation (26), and get the same relations as the flat interfaces.<sup>[10]</sup>

We can also get the spinodal points  $c_{s0}$ ,  $c_{s1}$  (assume  $c_{s0} < c_{s1}$ ) by letting the second derivatives of  $G_{lumped}$  to be zero. For flat interfaces, we have<sup>[10]</sup>

$$\frac{\partial \mu_h}{\partial c} \Big|_{c_{s0}} = \frac{\partial \mu_h}{\partial c} \Big|_{c_{s1}} = 0 \quad (28)$$

#### 3.2. Switching Current

In Ref. [26], we have derived an analytical estimation of the switching current above which MP occurs at least on one electrode, based on the 1D model for LTO memristors. This estimation is consistent with simulations. Here, we generalize the estimation for any forms of  $\mu_{k,chem}(c)$  and  $D_k(c)$ . Again, the estimation only works for 1D phase distribution (flat phase boundaries) and neutral wetting surfaces.

We first analyze the steady state concentration profiles in each phase below the switching current (see Figure S4, Supporting Information, in Ref. [26]). Here we neglect the defect concentration ( $c_d = 0$ ,  $c_p = c_n = c$ ). At steady state, the ion

diffusion and ion migration balance each other. Therefore, inside each phase, the current can be expressed as

$$i = \frac{D_n c F}{RT} \frac{\partial \mu_h}{\partial c} \frac{\partial c}{\partial x} = \frac{\partial \mathcal{F}(c)}{\partial x} \quad (29)$$

where  $\mathcal{F}(c) = \int \frac{D_n c F}{RT} \frac{\partial \mu_h}{\partial c} dc$ . This also directly indicates that current can induce CP inside each phase.

If CP is stronger enough to trigger phase separation on either electrode (the concentration reaches nearby spinodal point), MP occurs. We further assume that the concentration near the phase boundaries is still at binodal points. Therefore, the switching current can be estimated by

$$i_c^{ama} = \min \left\{ \frac{\mathcal{F}|_{c_{b0}}^{c_{b1}}}{\mathcal{O}(c_m)}, \frac{\mathcal{F}|_{c_{s1}}^{c_{s2}}}{L - \mathcal{O}(c_m)} \right\} \quad (30)$$

where  $\mathcal{O}(c_m) = \frac{c_{b1} - c_m}{c_{b1} - c_{b0}} L$  is the estimation of the spatial occupation of the ion-poor phase 0 when the average of  $c$  in the system is  $c_m$ .

### 3.3. Interfacial Energy and Thickness

In this part, we derive the energy density and estimate the thickness of the phase boundaries. The analysis is based on flat phase boundaries, but should still work for curved phase boundaries if the curvature radius is much larger than the interface thickness.

First, we obtain the concentration gradient perpendicular to a flat phase boundary (along coordinate  $x_i$ ) in equilibrium<sup>[47]</sup>:

$$\kappa_p \frac{\partial c}{\partial x_i} = \sqrt{2\kappa_p [g_h(c) - g_h(c_{b0}) - (c - c_{b0})\mu_b]} = \mathcal{I}(c) \quad (31)$$

by integrating

$$\mu_b \nabla c = (\mu_h - \kappa_p \nabla^2 c) \nabla c \quad (32)$$

along the coordinate  $x_i$ .

Then we calculate the interfacial energy of the phase boundary:

$$\gamma_i = \int_{-\infty}^{\infty} [g(c) - g_h(c_{b0}) - \mu_b(c - c_{b0})] dx_i \quad (33)$$

which can lead to<sup>[47]</sup>

$$\gamma_i = \int_{c_{b0}}^{c_{b1}} \mathcal{I}(c) dc \quad (34)$$

Using function  $\mathcal{I}(c)$ , we can also estimate the thickness of the phase boundary  $h_i$  from Equation (31), and get  $h_i \approx \kappa_p c_0 / \mathcal{I}(c_0/2)$ , where  $c_0$  is the characteristic concentration (maximum ion concentration) and  $c_0/2$  is approximately the concentration at the middle of the interface. Since the concentration gradient is largest at the middle of the interface, this expression should slightly underestimate  $h_i$ . In Section 5, we compare this estimation with simulations and find good agreement.

### 3.4. Contact Angle

In this part, we intend to analyze the effects of surface charge ( $C \neq 0$ ,  $\eta \neq 0$ ) and surface energy relaxation ( $\tau_\gamma > 0$ ) on MP, by analyzing the contact angle defined in the rich phase based on the gradient of  $c$ , as shown in Figure 3:

$$\frac{\mathbf{n} \cdot \nabla c}{|\nabla c|} = \cos \theta \quad (35)$$

Then we consider three contact angles:  $\theta_s^0$ , the static contact angle without overpotential;  $\theta_s$ , the static contact angle at overpotential  $\eta$ ;  $\theta_d$ , the dynamic contact angle. In the derivation, we assume that the concentration gradient perpendicular to the phase boundaries (Equation (31)) is not perturbed from the equilibrium state in any case. And we assume  $\frac{\partial C}{\partial c} = 0$  here for simplicity.

Without overpotential and surface relaxation ( $\tau_\gamma = 0$  and  $\eta = 0$ ), Equation 19b becomes

$$\frac{\partial \gamma_s^0}{\partial c} = -\mathcal{I}(c) \cos \theta_s^0 \quad (36)$$

Therefore, one additional parameter  $\theta_s^0$  is enough to give the wetting boundary condition. Obviously, the integral of this equation leads to the classical Young–Laplace equation (Equation (27)).

Next, we add an overpotential to the nanofilm-electrode interface ( $\tau_\gamma = 0$  but  $\eta \neq 0$ ). After plugging Equation (36) in Equation 19b, we obtain

$$\mathcal{I}(c)(\cos \theta_s - \cos \theta_s^0) + \frac{C\eta}{F} \frac{\partial \mu_{n,chem}}{\partial c} = 0 \quad (37)$$

Therefore, if we assume  $\frac{\partial \mu_{n,chem}}{\partial c} > 0$  (the Fermi energy lifts due to ion intercalation) and  $C \neq 0$ , we can deduce that:  $\eta > 0$  leads to  $\theta_s > \theta_s^0$ , which means that the positive electrode (the current goes from this electrode to the nanofilm) is less wetting to the rich phase due to the applied currents;  $\eta < 0$  leads to  $\theta_s < \theta_s^0$ , which means that the negative electrode (the current goes from the nanofilm to this electrode) is more wetting to the rich phase due to the applied currents.

Finally, we analyze the dynamic contact angle ( $\tau_\gamma > 0$  and  $\eta \neq 0$ ). We plug Equation (37) into Equation 19b and get

$$\mathcal{I}(c)(\cos \theta_d - \cos \theta_s) = -\tau_\gamma \frac{\partial c}{\partial t} \quad (38)$$

Therefore,  $\theta_d < \theta_s$  leads to  $\frac{\partial c}{\partial t} < 0$ , which means that the contact line moves to the rich phase (receding contact angle);  $\theta_d > \theta_s$  leads to  $\frac{\partial c}{\partial t} > 0$ , which means that the contact line moves to the poor phase (advancing contact angle).

### 3.5. Discussion on Electrowetting

In the previous part, we derive Equation (37) for the effect of surface charge and electric currents on static contact angle for our model system shown in Figure 2. In this part, we want to compare this effect to the well-known phenomenon of electrowetting for liquid droplets, which can also help to understand our problem.

In the classical setup for electrowetting, a droplet of aqueous salt solution is placed on a dielectric substrate, and a voltage is applied between an electrode wire in the droplet and the substrate. Then, people found that the voltage, regardless of sign, can make the dielectric more wetting to the droplet.<sup>[62–64]</sup> This phenomenon has been widely applied in microfluidics and “lab-on-a-chip” devices.

Apparently, this sign-independence of the voltage-tuned contact angle in electrowetting is not seen in the system of this study (according to Equation (37)), though the droplet in electrowetting is analogous to our more-conductive phase droplet (can be ion-rich or ion-poor phase depending on the material). The reason is that the two systems have different boundary conditions. Our system uses parallel electrodes, while electrowetting uses an electrode wire in the droplet and a substrate electrode. Therefore, in our system, the overpotential should be almost uniform on each electrode (since the nanofilm has small variation electrochemical potential if surface resistance dominates total resistance), while in electrowetting, the potential drop only occurs at the droplet-substrate interface.

If we modify our system by removing the top electrode and putting an electrode wire with no surface resistance in the rich phase droplet, assume that the rich phase is more conductive, neglect the charge at the interface between the poor phase and electrode, and consider the equilibrium state without leaky current (electron transfer at interfaces), then we get

$$\mathcal{G} = G_{\text{lumped}} - C\eta^2 A^{s,r} \quad (39)$$

where  $G_{\text{lumped}}$  is modified from Equation (25) by replacing  $\gamma_s^0(c^r)$  by  $\gamma_s(c^r) = \gamma_s^0(c^r) + \frac{1}{2}C\eta^2$  to include the electrostatic energy, and  $C\eta^2 A^{s,r}$  is the energy released from the voltage source. Then, the effective surface energy at the droplet-substrate surface now becomes  $\gamma_{s,r}^{\text{eff}} = \gamma_s^0(c^r) - \frac{1}{2}C\eta^2$ , which leads to the famous equation for electrowetting<sup>[62,65]</sup>

$$\cos\theta_s = \cos\theta_s^0 + \frac{C\eta^2}{2\gamma_i} \quad (40)$$

Note that the  $\eta$  that we define is the same as  $U - U_{pzc}$  in [62] ( $U$ : applied voltage, same as  $\Delta\phi$  in this work;  $U_{pzc}$ : applied voltage at point of zero charge, same as  $(\Delta\phi)_0$  in this work). Therefore, our phase field model is consistent with the electrowetting theory if the same boundary conditions and simplifications are applied.

In addition to boundary conditions, our system is also very different from the electrowetting system in the following aspects. First, our system is a pure solid system while electrowetting manipulates liquid droplets. Therefore, the phase field in our system can be represented by scaled ion concentration, while the phase field in electrowetting should be represented by scaled water concentration. Furthermore, the drag on the liquid droplet by electric fields should be weaker than that on the solid rich phase (ions only occupy a small fraction in liquid), so usually electrowetting neglects the body force on the droplet due to bulk electric fields. Finally, the leaky current at the nanofilm-electrode interface is very important in our system because it can lead to phase redistribution in the bulk, while in electrowetting the leaky current is usually avoided.

## 4. Nondimensionalization and Regular Solution Model

### 4.1. Dimensionless Governing Equations for the General Phase-Field Model

In this part, we summarize all the governing equations and boundary conditions in the dimensionless form. We define the scales of the variables as below: the concentration scale  $c_0 = c_p^{\text{max}}$ , the length scale  $L$  as the thickness of the nanofilm, the time scale as the diffusion time of ions  $\tau_D = L^2/D_p^0$ , the electrochemical potential scale  $RT$  ( $R$  is the gas constant and  $T$  is the temperature), the electric potential scale  $V_T = RT/F$  (thermal voltage), the free energy density scale  $RTc_0$ , the gradient energy coefficient scale  $\kappa_0 = L^2 RT/c_0$ , the interface energy density scale  $\gamma_0 = RTc_0 L$ , the capacitance density scale  $C_0 = Fc_0 L/V_T$ , the species flux scale  $J_{k,0} = D_k^0 c_0/L$  ( $D_k^0$  are constants chosen based on the material), the current scale  $i_D = J_{n,0} F$ , and the energy scale  $e_0 = i_D V_T \tau_D$ . Then we get the dimensionless variables by dividing the dimensional variables by the corresponding scales. Specifically, we also define  $\tilde{\mathcal{F}}(\tilde{c}) = \mathcal{F}(c)L/i_D$ ,  $\tilde{\mathcal{O}}(\tilde{c}_m) = \mathcal{O}(c_m)/L$  to non-dimensionalize Equation (51).

Now we can list the dimensionless governing equations:

$$\tilde{c}_p = \tilde{c}_n - \tilde{c}_d = \tilde{c} \quad (41)$$

$$r_k \frac{\partial \tilde{c}_k}{\partial \tilde{t}} + \tilde{\nabla} \cdot \tilde{\mathbf{j}}_k = 0, \quad \tilde{\mathbf{j}}_k = -\tilde{D}_k \tilde{c}_k \tilde{\nabla} \tilde{\mu}_k, \quad (k = p, n) \quad (42)$$

where  $\tilde{\nabla} = L\nabla$ ,  $r_p = 1$ ,  $r_n = D_p^0/D_n^0$ . And  $\tilde{\mu}_k$  is the scaled electrochemical potential

$$\tilde{\mu}_k = \tilde{\mu}_{k,\text{chem}} + z_k \tilde{\phi} - \tilde{\kappa}_k \tilde{\nabla}^2 \tilde{c} \quad (43)$$

where we assume  $\tilde{\kappa}_n = 0$ .

Next we list the boundary conditions. We put the electrodes on coordinates  $\tilde{y} = 0$  and  $\tilde{y} = 1$ , where

$$\tilde{\mathbf{j}}_p \cdot \mathbf{n} = 0 \quad (44a)$$

$$\tilde{\mathbf{j}}_n \cdot \mathbf{n} = -\mathbf{n} \cdot \tilde{\mathbf{i}} = \tilde{J}_n^{\text{ET}}(\tilde{c}, \tilde{\eta}) + \tilde{C} \frac{\partial \Delta \tilde{\phi}}{\partial \tilde{t}} \quad (44b)$$

$$\tilde{\kappa}_p \tilde{\nabla} \tilde{c} \cdot \mathbf{n} = -\tilde{\tau}_\gamma \frac{\partial \tilde{c}}{\partial \tilde{t}} + \tilde{\mathcal{I}}(\tilde{c}) \cos\theta_s^0 - \tilde{C} \tilde{\eta} \frac{\partial \tilde{\mu}_{n,\text{chem}}}{\partial \tilde{c}} \quad (44c)$$

where  $\tilde{\mathcal{I}}(\tilde{c})$  has the following expression

$$\tilde{\mathcal{I}}(\tilde{c}) = \sqrt{2\tilde{\kappa}_p [\tilde{g}_h(\tilde{c}) - \tilde{g}_h(\tilde{c}_{b0}) - (\tilde{c} - \tilde{c}_{b0})\tilde{\mu}_b]} \quad (45)$$

and  $\tilde{J}_n^{\text{ET}}(\tilde{c}, \tilde{\eta})$  is given in Section 4.2. Finally, we close the domain with two symmetric boundaries on  $\tilde{x} = 0$  and  $\tilde{x} = W/L$  where

$$\tilde{\mathbf{j}}_n \cdot \mathbf{n} = 0, \quad \tilde{\mathbf{j}}_p \cdot \mathbf{n} = 0, \quad \tilde{\nabla} \tilde{c} \cdot \mathbf{n} = 0 \quad (46)$$

### 4.2. Constitutive Equations for a Regular Solution

Up to now, our phase-field model is general and can be applied to any form of  $D_p(\tilde{c})$ ,  $D_n(\tilde{c})$ ,  $\mu_{p,\text{chem}}(\tilde{c})$ ,  $\mu_{n,\text{chem}}(\tilde{c})$ , and  $J_n^{\text{ET}}(\tilde{c}, \tilde{\eta})$ . Now we want to specify the above functions for a regular solution model and use them for simulations in the next section. In



addition, we also derive  $\tilde{\mathcal{F}}(\tilde{c})$  for the regular solution model to get the switching current.

In the regular solution model, we consider both electrons and ions as Fermi-Dirac particles hopping on specific lattices and experiencing some interaction energy. This model for ions (or ion-electron pairs) has been widely used.<sup>[12]</sup> For electrons, this model should also work well for many ion-intercalation materials where mobile electrons are usually localized on transition metal atoms and the electronic conduction is mainly due to electron hopping<sup>[66–69]</sup> but not band conduction.<sup>[57]</sup> Therefore, we can assume<sup>[12,26]</sup>

$$\tilde{D}_k = 1 - \frac{\tilde{c}}{\tilde{c}_k^{\max}} \quad (47)$$

and

$$\tilde{\mu}_k = \ln \frac{\tilde{c}_k}{\tilde{c}_k^{\max} - \tilde{c}_k} + \tilde{\mu}_k^0 + \Omega_k (\tilde{c} + \rho \tilde{c} (1 - \tilde{c})) \quad (48)$$

where  $\tilde{c}_k^{\max}$  is the maximum available sites for ions or electrons to sit in,  $\Omega_k$  controls the magnitude of interaction energy, and  $\rho$  helps control the symmetry of the phase diagram. We further define  $\Omega = \Omega_p + \Omega_n$ , which is a key parameter to determine  $\mu_h$ .  $\tilde{c}_k^{\max}$  may be different for ions and electrons. For example, we assume  $\tilde{c}_n^{\max}/\tilde{c}_p^{\max} = 5/3$  in our LTO model in Ref. [26] according to the available space for ions to intercalate in and the Ti atoms for electrons to hop on. In this case, the ion-rich phase is more electronically conductive.

Since we assume the mobile electrons are localized, the electron transfer can be seen as Faraday reaction (e.g.,  $Ti^{4+} + e^- (Pt) \rightleftharpoons Ti^{3+}$  for LTO memristors). We then apply the generalized, empirical Butler–Volmer equation for electron transfer kinetics (see details in Ref. [26])

$$\tilde{J}_n^{ET}(\tilde{c}, \tilde{\eta}) = D \alpha f(\tilde{c}; \alpha) g(\tilde{\eta}_{eff}; \alpha) \quad (49a)$$

$$f(\tilde{c}; \alpha) = (\tilde{c}_n / \tilde{c}_n^{\max})^\alpha (1 - \tilde{c}_n / \tilde{c}_n^{\max})^{1-\alpha} e^{\alpha \Omega_n (\tilde{c} + \rho \tilde{c} (1 - \tilde{c}))} \quad (49b)$$

$$g(\tilde{\eta}_{eff}; \alpha) = e^{(1-\alpha)\tilde{\eta}_{eff}} - e^{-\alpha\tilde{\eta}_{eff}} \quad (49c)$$

where the effective overpotential  $\tilde{\eta}_{eff}$  only works on the electron transfer dynamics, excluding the voltage loss on the series resistance or film resistance<sup>[70]</sup>

$$\tilde{\eta}_{eff} = \tilde{\eta} - \tilde{J}_n^{ET} \tilde{R}_s \quad (50)$$

Therefore, if  $\Omega_n > 0$ , which indicates that the Fermi energy increases as more ions are intercalated, the electron transfer rate increases almost exponentially with  $c$ .

Finally, we calculate  $\tilde{\mathcal{F}}(\tilde{c})$  based on the regular solution model, and get

$$\mathcal{F} = \left( 1 + \frac{\tilde{c}_p^{\max}}{\tilde{c}_n^{\max}} \right) \tilde{c} - \tilde{c}_p^{\max} \left( 1 - \frac{\tilde{c}_p^{\max}}{\tilde{c}_n^{\max}} \right) \ln \left( 1 - \frac{\tilde{c}}{\tilde{c}_p^{\max}} \right) + \Omega (1 + \rho) \left( \frac{\tilde{c}^2}{2} - \frac{\tilde{c}^3}{3\tilde{c}_n^{\max}} \right) - 2\Omega\rho \left( \frac{\tilde{c}^3}{3} - \frac{\tilde{c}^4}{4\tilde{c}_n^{\max}} \right) \quad (51)$$

which can be plugged in the non-dimensional form of Equation (30) to calculate the switching current  $\tilde{i}_c^{ana}$ .

## 5. Numerical Simulation

### 5.1. Simulation Method and Setup

#### 5.1.1. Numerical Method

In this part, we perform simulations on the equations summarized in Section 4. We discretize the equations using finite volume method, which ensures species conservation, and use the convex splitting method to get an unconditionally stable time marching scheme.<sup>[71,72]</sup> Note that we do convex splitting not only for bulk energy but also for surface energy.<sup>[73]</sup> We also use adaptive time stepping to save the computational time without losing the accuracy.<sup>[74,75]</sup> Finally, we implement the method in MATLAB R2022a. We use the automatic differentiation package developed by Gorce<sup>[76]</sup> to calculate the Jacobian.

#### 5.1.2. Parameters

For all the simulation cases presented in this paper, we assume the nanofilm has thickness  $L = 50$  nm, and let  $\tilde{\kappa}_p = 0.0014$  so that the phase boundary thickness  $h_f \approx \sqrt{\tilde{\kappa}_p / \tilde{L}} (0.5)L \approx 2.1$  nm. This estimation is much more accurate than the scaling analysis  $h_f \approx \sqrt{\tilde{\kappa}_p / |\Omega|} L = 0.54$  nm.<sup>[12]</sup> The simulation domain is  $\tilde{x} \in [0, 2]$  (the direction parallel to the electrodes,  $W/L = 2$ ) and  $\tilde{y} \in [0, 1]$  (the direction perpendicular to the electrodes). We put 200 volumes in the  $x$  direction and 100 volumes in the  $y$  direction, so that there are at least 5 points in the phase boundary.

Though our theory is general, we need to parameterize  $\tilde{\mu}_k$  and  $\tilde{J}_n^{ET}(\tilde{c}, \tilde{\eta})$  to run simulations. We use the regular solution model and choose the following parameters based on the LTO material, as we did in the previous paper<sup>[26]</sup>:  $\tilde{c}_p^{\max} = 1$ ,  $\tilde{c}_n^{\max} = 5/3$ ,  $\Omega_n = 20$ ,  $\Omega_p = -32$ ,  $D_p = 1 \times 10^{-16}$  m<sup>2</sup> s<sup>-1</sup>,  $D_n = 1 \times 10^{-11}$  m<sup>2</sup> s<sup>-1</sup>,  $c_0 = 22.8$  M,  $\tilde{c}_d = 0.01$ ,  $\tilde{R}_s = 100$ . In addition, we choose  $\rho = 0.4$  to adjust the symmetry of the phase diagram. For the electron transfer, we assume symmetric transfer  $\alpha^T = \alpha^B = 0.5$ , and choose  $Da^T = 1 \times 10^{-2}$  and  $Da^B = 1 \times 10^{-4}$  unless specified. Finally, when we want to consider dynamic contact angle, we set  $\tilde{\tau}_\gamma = 0.02$ ; when we want to consider surface charge, we take  $C = \frac{10\epsilon_0}{1 \text{ nm}} = 0.0885$  C V<sup>-1</sup> m<sup>-2</sup> so that  $\tilde{C} = 2.07 \times 10^{-5}$ .

Based on the above parameters, we can derive the following properties of the material. (1) The dimensional scales are  $\tau_D = 25$  s,  $J_p^0 = 4.56 \times 10^{-5}$  mol s<sup>-1</sup> m<sup>-2</sup>,  $J_n^0 = 4.56$  mol s<sup>-1</sup> m<sup>-2</sup>,  $i_D = 4.4 \times 10^5$  A m<sup>-2</sup>,  $\gamma_0 = 2.83$  N m<sup>-1</sup>. The surface energy of the phase boundaries is  $\tilde{\lambda}_i = 0.023$ . (2) For phase equilibrium, we have  $\tilde{c}_{b0} = 0.0265$ ,  $\tilde{c}_{b1} = 0.9733$ ,  $\tilde{c}_{s0} = 0.1422$ , and  $\tilde{c}_{s1} = 0.8135$  for flat phase boundaries. Then the perturbation of the interface curvature to the binodal points and spinodal points is within 10% for droplets with curvature radius bigger than 10 nm. For example,  $r_0/L = 0.314$  leads to  $\tilde{c}_{b0} = 0.0280$ ,  $\tilde{c}_{b1} = 0.9754$ , and  $r_0/L = -0.314$  leads to  $\tilde{c}_{b0} = 0.0250$ ,  $\tilde{c}_{b1} = 0.9708$ . The error between these predictions and simulations is within 0.05%. (3) Next, we can analyze the transport behaviors. The ionic conductivity scales with  $\tilde{c}(1 - \tilde{c})$ , and the ionic tracer diffusivity  $D_p = D_p^0(1 - \tilde{c})$  decreases with  $c$ . Since  $\tilde{c}_n^{\max} = 5/3$  and the electronic conductivity scales with  $\tilde{c}(1 - \tilde{c}/\tilde{c}_n^{\max})$ , the material experiences insulator-metal transition as concentration increases.

In addition, since  $\Omega_n > 0$ , the electron transfer between the ion-rich phase and electrodes feels less resistance, compared with that between the ion-poor phase and the electrodes. (4) Finally, curves of  $\tilde{\mu}_h(\tilde{c})$ ,  $\tilde{I}(\tilde{c})$  and  $\tilde{i}_c^{ana}(\tilde{c})$  for these given parameters can be found in Figure S1, Supporting Information, (some other parameters are also plotted for a comparison). We estimate the switching current for flat phase boundaries and neutral wetting condition, and get  $\tilde{i}_c^{ana}(0.1) = 0.0975$ ,  $\tilde{i}_c^{ana}(0.9) = 0.5310$ .

### 5.1.3. Simulation Plan

In this paper, we consider two mean concentrations  $\tilde{c}_m = 0.1, 0.9$ . Both  $\tilde{c}_m$  enable phase separation since they are between the binodal points. In systems with  $\tilde{c}_m = 0.1$  ( $\tilde{c}_m = 0.9$ ), there is a thin film or small droplet of the more-conductive ion-rich phase (less-conductive ion-poor phase) surrounded by the less-conductive ion-poor phase (more-conductive ion-rich phase).

For each  $\tilde{c}_m$ , we consider two processes. We first simulate the response of the system to a step current (set total current and assume each electrode has uniform potential), to present the time evolution of phase boundaries and obtain the switching current, time, and energy. As shown in Section 3, 1D MP is controlled by currents but not total voltage drop. In the current response, the electron transfer kinetics do not matter at all for 1D MP without surface charge<sup>[26]</sup> (electron transfer kinetics is critical for MP-induced RS but not MP itself). Ion-modulated electron transfer can influence the current density distribution on electrodes for 2D phase distribution, and can also influence the overpotential magnitude and thus influence the surface energy if surface charge exists. Then we simulate the process of cyclic voltammetry and show the non-volatile RS behaviors. In this process, electron transfer kinetics is important for all the cases. In the step current simulation, we first let the system relax for dimensionless time of 5, then apply a constant current for  $0 \leq \tilde{t} < 5$ , and finally remove the current and let the system relax for  $5 \leq \tilde{t} < 25$ . In the cyclic voltammetry simulation, we first let the system relax for dimensionless time of 2, and then run three cycles at voltage sweeping rate  $2V_T \text{ s}^{-1}$ . Then we only plot results for the last cycle.

Finally, for each  $\tilde{c}_m$  and each process, we consider seven cases with six sets of boundary conditions and two initial conditions. We first choose a base case with flat initial phase boundaries, uniform surface resistance, neutral wetting, no surface charge and no surface relaxation. The base case can be seen as a 2D simulation of the 1D problem in Ref. [26]. Then we modify the base case by implementing curved initial phase boundaries, heterogeneous surface resistance, heterogeneous wetting condition (wetting nuclei), surface energy relaxation, surface charge, and complete wetting condition (completely wetting to one phase), and get six other cases. Therefore we can analyze each effect separately. Note that we add the complete wetting case, because solid interfaces are likely to show complete wetting instead of finite contact angle.<sup>[77]</sup> The parameters for the seven cases are listed in Figure 4 and Figure 7. When adding wetting nuclei, we use  $\theta_s^0 = \frac{\pi}{2} (1 \pm e^{-2((\tilde{x}-1)/0.05)^2})$ , where “+” (“-”) is used to make the nuclei completely wetting to the poor (rich) phase.

## 5.2. Simulation Results for the Ion-Poor System

In this part, we present results for the ion-poor system ( $\tilde{c}_m = 0.1$ ). We place the rich phase near the top electrode initially, and expect that the rich phase can be moved to the bottom at high enough electric currents.

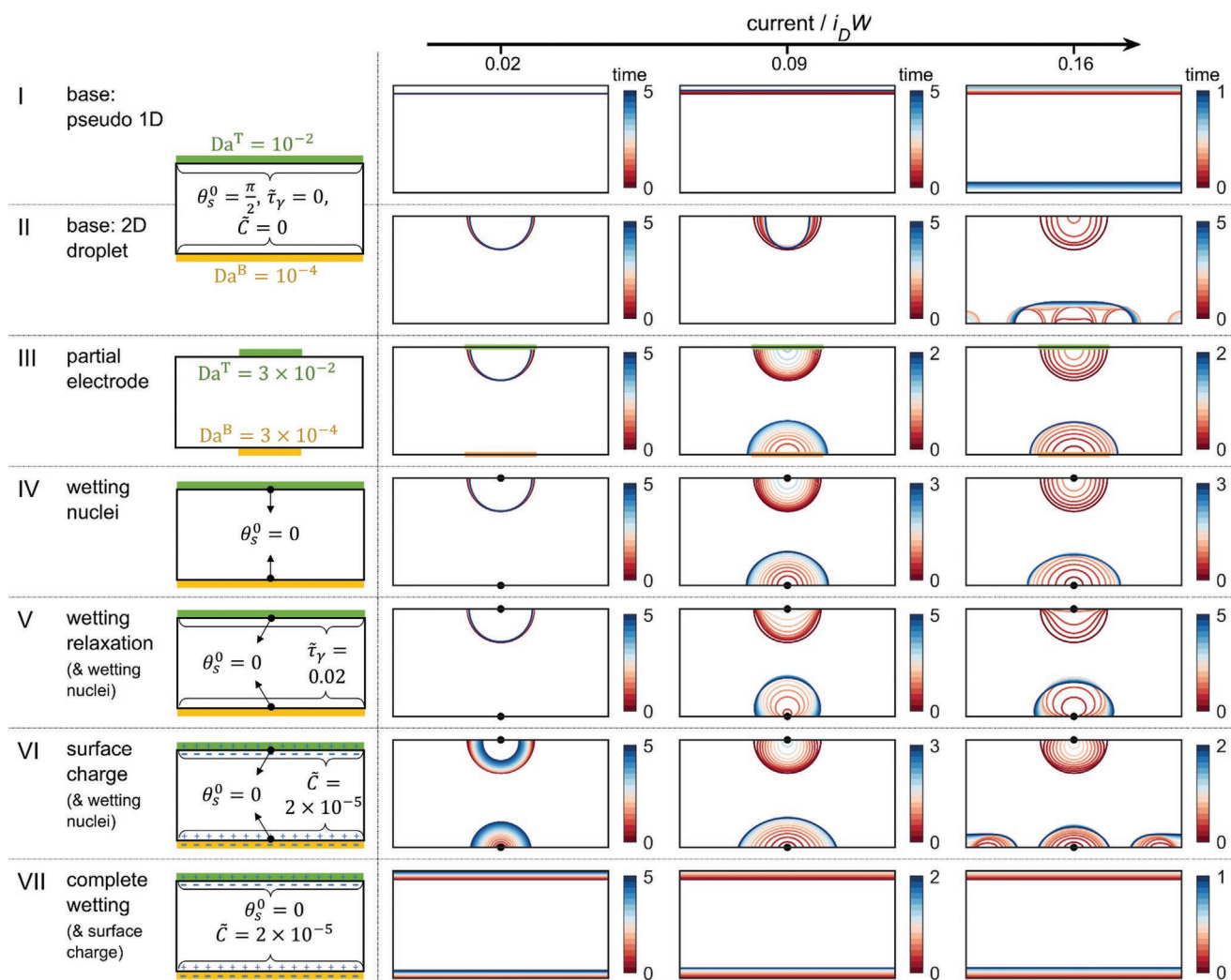
### 5.2.1. Time Evolution of Phase Boundaries and Interfacial Concentration

Figure 4 shows the time evolution of phase boundaries in response to a step current. We only present the time periods after the application of current and before the completion of IPC on both electrodes (see Figure 5 and Section 5.2.2 for detailed time analysis).

First, we can see that only high enough currents can trigger phase redistribution (MP). Then we compare different cases. For case I, II with the same homogeneous boundary conditions, as the current is applied, the flat initial phase boundaries maintain flat (case I), while the curved initial phase boundaries maintain curved (case II). Without surface heterogeneity, the rich phase nucleation can occur at random, multiple locations (case II, current = 0.16). The heterogeneous electron transfer resistance (partial electrode, case III) and heterogeneous wetting condition (wetting nuclei, case IV) can make phase nucleation easier to occur and preferable to occur at certain locations (centers in case III, IV). Also note that in case II, III, IV, the contact angle is always 90 degrees on electrodes where we apply the static neutral wetting condition ( $\nabla c \cdot \mathbf{n} = 0$ , except in the nuclei in IV). As we add the wetting relaxation in case V, we get the advancing contact angle ( $\theta_a > \pi/2$ ) on the bottom electrode, and the receding angle ( $\theta_r < \pi/2$ ) on the top electrode. As we add a surface charge capacity in case VI (but no wetting relaxation), we find that the top electrode with positive overpotential becomes less wetting to the rich phase, which supports the detachment of the rich-phase droplet, while the bottom electrode with negative overpotential becomes more wetting to the rich phase, which supports the nucleation of the rich-phase (may occur at multiple locations). This is consistent with our analysis for Equation (37), and indicates that the surface charge makes MP easier to occur if  $\frac{\partial \mu_{n,chem}}{\partial c} > 0$ . Finally, we find that the completely wetting surface (wetting to the rich phase) also makes MP easier to occur (case VII), similar to the effects of the wetting nuclei (case VI).

Then we use Figure 5a to quantitatively compare the mean interfacial concentration along with time for different cases at current 0.16. As we can see, different cases show very different curve patterns. For example, the pseudo-1D phase distribution in case I and case VII leads to the most abrupt IPC (steepest slope during switching), while the wetting relaxation in case V leads to slowest IPC. Basically, this model opens the opportunity to potentially learn the physics of MP using only the information for interfacial concentration evolution.

We also plot time evolution of interfacial concentration and applied voltage at different currents for each case in Figures S2 and S3 (Supporting Information), where the relaxation period after the removal of current is also included. Figure S2



**Figure 4.** Time ( $\tilde{t} = t/\tau_D$ ) evolution of the phase boundaries (contour lines of  $\tilde{c} = 0.5$ ) in the ion-poor systems (mean concentration  $\tilde{c}_m = 0.1$ ) after applying constant electric currents ( $\tilde{I} = I/i_D W$ , where  $I = \int_0^W i dx$ ), for three currents and seven cases. A sufficiently large downward current can move the ion-rich film or droplet from the top electrode to the bottom. Case I and II has the same boundary conditions but different initial phase boundaries. Case I can be seen as 2D simulations of the 1D problems in Ref. [26]. Case III–VII have one or two boundary conditions different from I and II, as described in the left column. The corresponding animations of concentration and electric potential profiles can be found in Movie S1 and Movie S2.

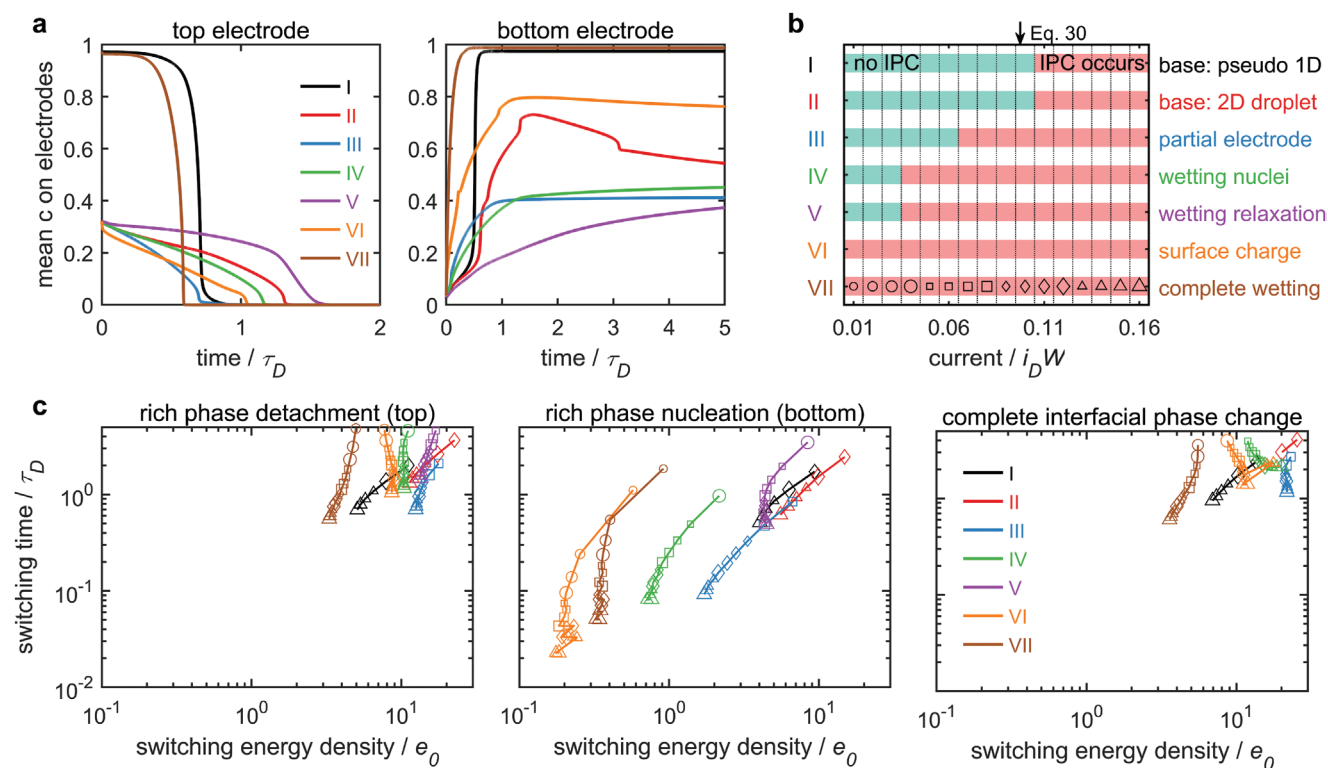
(Supporting Information) shows clearly that IPC only occurs if the concentration near at least one electrode goes through a spinodal point. Also, we can see that the IPC is non-volatile as long as MP completes during the application of the current, and the increased current accelerates the process.

### 5.2.2. Switching Current, Time, and Energy

In this part, we fill in more simulations for series of currents, and obtain the switching current, time, and energy. We identify three critical events for MP-induced IPC: (1) the completion of the detachment of the rich phase film/droplet from the top electrode judged from  $\max(\tilde{c}|_{\tilde{x}=1}) < 0.5$ , (2) the start of the nucleation of the rich phase on the bottom judged from  $\max(\tilde{c}|_{\tilde{x}=0}) > 0.5$ , and (3) the completion of IPC judged from the slope

of the time evolution of mean interfacial concentration  $\sqrt{[(\partial\langle\tilde{c}|_{\tilde{x}=0}\rangle/\partial\tilde{t})^2 + (\partial\langle\tilde{c}|_{\tilde{x}=1}\rangle/\partial\tilde{t})^2]}/2 \leq 0.01$ . If at least one of the first two events occur, we say that IPC and MP occurs at the given current, and call the corresponding threshold current as the switching current. Then we define three switching times as the time spent respectively for the three events to occur during the application of the current. Note that the switching time has definition only if the corresponding event occurs. We show the switching current for different cases in Figure 5b, and show the switching time versus energy in Figure 5c.

First, we can see from Figure 5b that the switching current indicated by simulations for the pseudo-1D base system is well consistent with our analytical prediction (Equation (30)), which has been well studied in our previous work.<sup>[26]</sup> Then we can analyze the differences between the 1D and 2D pictures. By comparing case I with II, and case IV with V, we find the initial



**Figure 5.** Characterization of the MP-induced interfacial phase change (IPC) in the ion-poor systems shown in Figure 4. a) Time ( $\tilde{t} = t/\tau_D$ ) evolution of the mean ion concentration on electrodes at current  $\tilde{I} = I/i_D W = 0.16$ . b) Switching current ( $\tilde{I}_s$ ) obtained by checking whether IPC occurs at least on one electrode in the simulations. The arrow shows the analytical switching current for case I from Equation (30). c) Switching time ( $\tilde{t}_s$ ) along with energy density ( $\tilde{e} = e/e_0 = \int_0^{\tilde{t}_s} \tilde{V} d\tilde{t}$ ) characterized by three events: the completion of the detachment of the rich phase from the top electrode, the initiation of the nucleation of the rich phase on the bottom electrode, and the completion of IPC on both electrodes. The markers in (c) represent different currents, which are consistent with those shown at the bottom of (b). The dimensional scales (values for a 50-nm-thick LTO film) are:  $\tau_D = L^2/D_p^0$  (25 s),  $i_D = D_p^0 F c_0/L$  ( $0.44 \mu\text{A} \mu\text{m}^{-2}$ ),  $e_0 = i_D V \tau_D$  ( $0.275 \mu\text{J} \mu\text{m}^{-2}$ ).

condition and wetting relaxation do not matter for the switching current. Then by comparing case II with III and IV, and case IV with VI and VII, we find that the heterogeneity of the boundary conditions, the surface charge, and the complete wetting condition can reduce the switching current significantly.

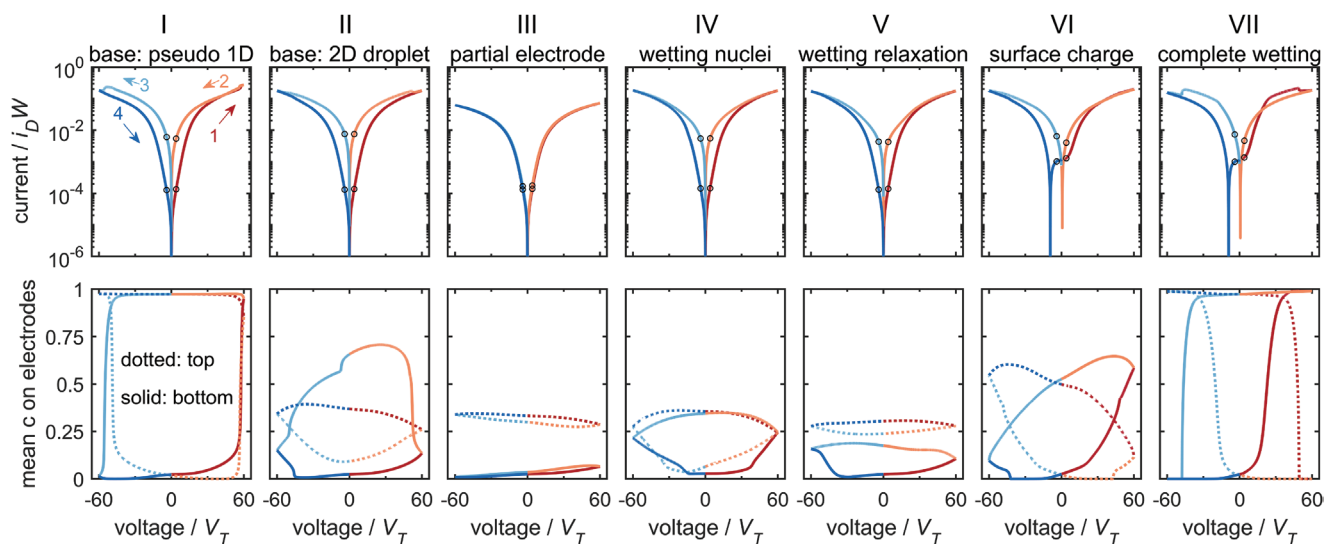
Next, we discuss the switching time for each case shown in Figure 5c. Generally, the switching time is dominated by ion diffusion and can be reduced by increasing the current. Regardless of the existence of the wetting nuclei, the nucleation of the rich phase on the bottom occurs earlier in time than the detachment of the rich phase from the top at the given current. Complete IPC and rich phase detachment from the top take similar time, and the complete wetting condition (case VII) takes smallest time among all the cases for complete IPC and rich phase detachment. The increasing current can reduce the switching time by nearly one magnitude for rich phase detachment and complete IPC, and nearly two magnitudes for rich phase nucleation.

Then we discuss the switching energy for each case shown in Figure 5c. The switching energy density is mainly determined by the ion diffusion time multiplied by the electron diffusion current. Since the inverse of switching time should be roughly proportional to the excess current (current minus switching current),<sup>[26]</sup> the switching energy may decrease with

current at small currents, and should not change much with current at large currents. Sometimes the switching energy can also increase with current if multiple nucleation points start to appear. The switching energy is much smaller for the rich phase nucleation compared with rich phase detachment and complete IPC. By increasing current, the switching energy does not change much with current for rich phase detachment and complete IPC, but can decrease significantly for rich phase nucleation. We can also compare the dimensional numbers with experiments. If we assume the switching energy density is  $e_0$ , we predict that the switching energy for a  $100 \mu\text{m} \times 100 \mu\text{m}$  device is around 1 mJ, while the experimental value is around 0.1 mJ ( $(4\text{V})^2 \times 0.8 \mu\text{J} \times 50 \times 500 \text{ms}$ , for 50 pulses in Figure 2c of Ref. [5]). These two values are pretty close, considering that the electronic conductivity varies greatly in solid devices (e.g., see Ref. [78]).

Furthermore, we compare different cases for switching time and energy in Figure 5. We find that partial electrode (case III), wetting nuclei (case IV), surface charge (case VI), and complete wetting (case VII) can reduce the time and energy for rich phase nucleation very significantly compared with the base case (case I), while the wetting relaxation (case V) can slow down the switching.

Finally, the above analysis for the three events of IPC is limited to  $\tilde{c}_m = 0.1$ . We can imagine that if we further decrease the



**Figure 6.** Current ( $\tilde{i} = I/i_D W$ , top row) and mean concentration on electrodes (bottom row) along with the applied voltage ( $\tilde{V} = V/V_T$ , where  $V_T = 0.025$  V) during cyclic voltammetry with voltage sweeping rate 50 (scaled by  $V_T/\tau_D$ ), for the ion-poor systems shown in Figure 4. The circles on the current-voltage curves mark the points with  $|V| = 4$ , which guide the eyes to read the resistance ratio. The dimensional scales (values for a 50-nm-thick LTO film) are:  $\tau_D = L^2/D_p$  (25 s),  $i_D = D_p^0 F c_0 / L$  ( $0.44 \mu\text{A} \mu\text{m}^{-2}$ ). The corresponding time evolution of concentration contour maps can be found in Movie S3.

mean concentration (still above  $c_{b0}$ ), the time and energy for complete IPC and rich-phase detachment should decrease and become closer to those for rich-phase nucleation.

### 5.2.3. Resistive Switching

Finally, we discuss on the memristive switching behaviors of the ion-poor system due to MP-induced IPC. The simulation results for cyclic voltammetry with a maximum voltage magnitude of 60 is shown in Figure 6. Since the bottom electrode is assumed to have smaller  $Da$ , it should have smaller electron transfer rate given the same  $\tilde{c}$  and  $\tilde{\eta}$ . In addition, the electron transfer rate also increases with  $\tilde{c}$  since we assume positive  $\Omega_r$ . Therefore, we expect that the migration of the rich phase droplet/film from the top electrode to the bottom should reduce the overall resistance. In another word, the nonvolatile IPC can lead to nonvolatile resistive switching.

The results shown in Figure 6 is consistent with the above expectation. For all the cases, no matter the rich phase exists as a droplet or a film, RS occurs as long as IPC occurs. The current-voltage curve in case I is consistent with our 1D simulations in the previous paper.<sup>[26]</sup> When surface charge exists (case VI, VII), the current-voltage curves show hysteretic behaviors (zero current occurs at non-zero voltage). In addition, we can see that the wetting nuclei (case IV), surface charge (case VI), and complete wetting condition (case VII) can make IPC occur earlier (at smaller voltage).

## 5.3. Simulation Results for the Ion-Rich System

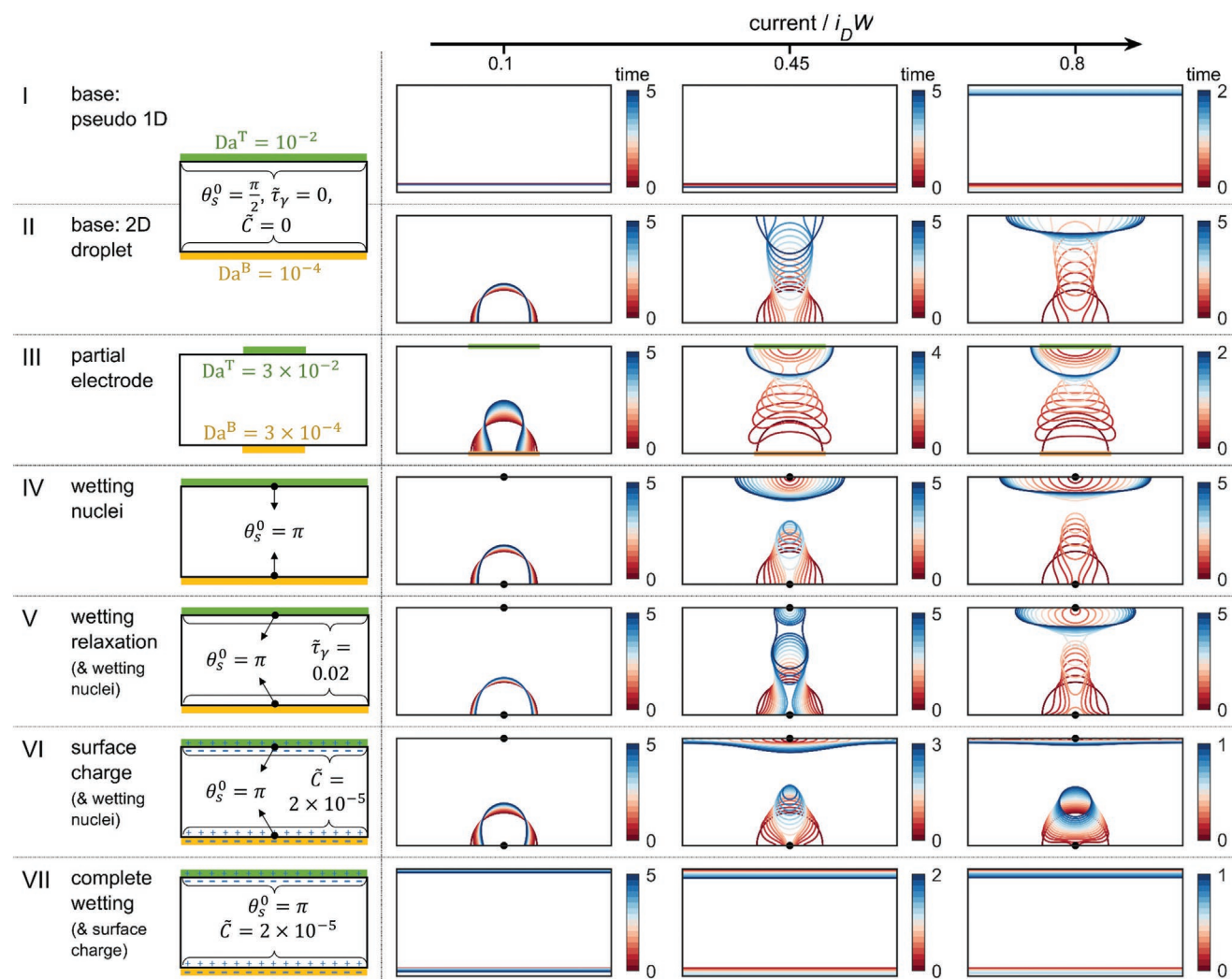
In this part, we present results for the ion-rich system ( $\tilde{c}_m = 0.9$ ). We initially place the poor phase on the bottom electrode, and

expect that the poor phase can be moved to the top at high enough currents. Since the ion-poor system has been discussed before, here we mainly focus on the different behaviors between the ion-poor system and the ion-rich system. These differences should come from the asymmetry between ion transport and electron transport, as described in Section 5.1.2.

### 5.3.1. Time Evolution of Phase Boundaries and Interfacial Concentration

As we can see in Figure 7, MP in the ion-rich systems needs larger current than the ion-poor systems, and the time evolution of phase boundaries is very different. When there is no wetting nuclei (case II, III), the poor-phase droplet first detaches completely from the bottom electrode, and then migrates to the top electrode. However, in case II and III for the ion-poor systems and case IV, V, VI for both ion-poor and ion-rich systems, the droplet detachment and nucleation can occur at the same time. In addition, we find that the surface charge in case VI also makes MP easier to occur in the ion-rich system. During the application of the current, the bottom electrodes become less wetting to the ion-poor phase, which helps the detachment of the droplet; while the top electrode becomes more wetting to the ion-poor phase, which helps the nucleation of the droplet. In addition, we find that the large currents plus the surface charge can squeeze the droplet to a film on the top electrodes. Finally, the complete wetting surface (wetting to the poor phase) can also help MP to occur.

The time evolution of the mean concentration on electrodes for the ion-rich system shown in Figure 8a and Figure S4 (Supporting Information) is similar to that for the ion-poor system. However, during the application of the current, the mean concentration on the top in case II, IV, V, VI



**Figure 7.** Time ( $\tilde{t} = t/\tau_D$ ) evolution of the phase boundaries (contour lines of  $\tilde{c} = 0.5$ ) in the ion-rich systems (mean concentration  $\tilde{c}_m = 0.9$ ) after applying constant currents ( $\tilde{I} = I/i_D W$ , where  $I = \int_0^w id_x$ ), for three currents and seven cases. A sufficiently large downward current can move the poor phase film or droplet from the bottom electrode to the top. Case I and II has the same boundary conditions but different initial phase boundaries. Case I can be seen as 2D simulations of the 1D problems in Ref. [26]. Case III–VII have one or two boundary conditions different from I and II, as described in the left column. The corresponding animations of concentration and electric potential profiles can be found in Movie S4 and Movie S5.

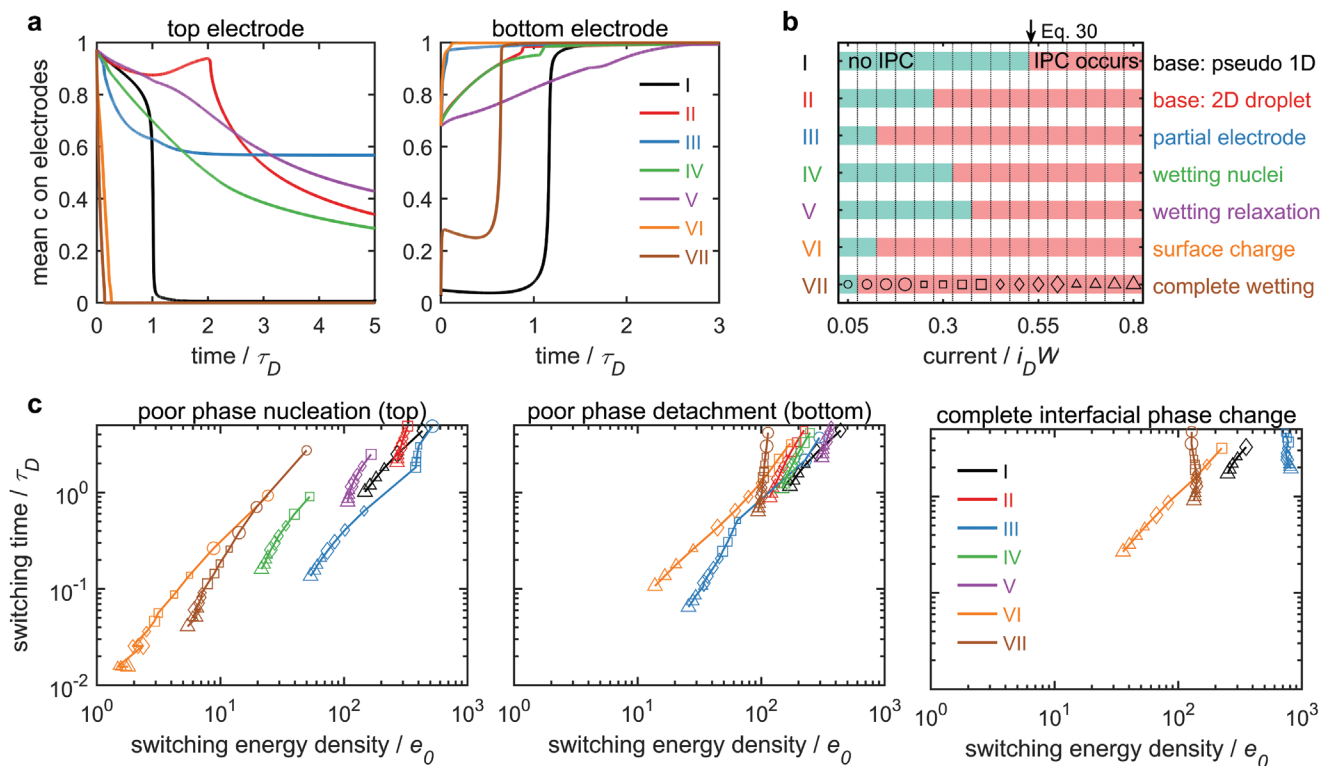
can increase more significantly due to the squeezing of the droplets by the large current. The squeezed droplets can rebound after the current is removed if the droplets have not been squeezed into a film (case II, IV, V), making the relaxation require longer time (Figures S4 and S5, Supporting Information).

### 5.3.2. Switching Current, Time, and Energy

We define the switching current and times for the ion-rich systems similar to what we do for the ion-poor systems. Here we judge the full detachment of the poor phase from the bottom from  $\min(\tilde{c}|_{\tilde{x}=0}) > 0.5$ , and the start of the poor phase nucleation on the top from  $\min(\tilde{c}|_{\tilde{x}=1}) < 0.5$ . If one of the above two events occurs, we say that MP and IPC occurs.

As shown in Figure 8, MP in the ion-rich system needs about 5 times larger switching current than the ion-poor system, as predicted by both the theory and simulations. By comparing case I and II, we find that the 2D poor-phase droplet is easier to detach from the bottom and nucleate on the top compared with the poor-phase film. The surface heterogeneity in case III and IV, surface charge in case VI, and complete wetting in case VII can also reduce the switching current.

Then we discuss the switching time and energy shown in Figure 8c. The poor-phase droplet detachment from the bottom can occur earlier in time than the poor-phase droplet nucleation on the top if the electrodes have neutral wetting condition (case II, III). Otherwise, nucleation is always earlier than detachment. The significant squeezing of the droplets before the formation of films in case II, IV, V increases the time to complete IPC (longer than the step current time). Once the



**Figure 8.** Characterization of the MP-induced interfacial phase change (IPC) in the ion-rich systems shown in Figure 7. a) Time ( $\tilde{t} = t/\tau_D$ ) evolution of the mean ion concentration on electrodes at current  $\tilde{I} = I/i_D W = 0.8$ . b) Switching current ( $I_s$ ) obtained by checking whether IPC occurs at least on one electrode in the simulations. The arrow shows the analytical switching current for case I from Equation (30). c) Switching time ( $\tilde{t}_s$ ) along with energy density ( $\tilde{e} = e/e_0 = \int_0^{\tilde{t}} \tilde{I} d\tilde{t}$ ) characterized by three events: the initiation of the nucleation of the poor phase on the top electrode, the completion of the detachment of the poor phase from the bottom electrode, and the completion of IPC on both electrodes. The markers in (c) represent different currents, which are consistent with those shown at the bottom of (b). The dimensional scales (values for a 50-nm-thick LTO film) are:  $\tau_D = L^2/D_p^0$  (25 s),  $i_D = D_p^0 F c_0 / L$  ( $0.44 \mu\text{A} \mu\text{m}^{-2}$ ),  $e_0 = i_D V_T \tau_D$  ( $0.275 \mu\text{J} \mu\text{m}^{-2}$ ).

droplet is squeezed into a film on the top (case VI), IPC takes much shorter time and energy. In case VI, after the completion of IPC, there may still exist the migration of the poor phase in the system, but the interfacial concentration does not change anymore, as shown in Figure 7.

### 5.3.3. Resistive Switching

Unlike the ion-poor system, a less-conductive poor-phase droplet in the ion-rich system may not change the interfacial resistance on each electrode significantly. To make a big change, the poor phase needs to cover the whole electrode, or the very conductive points for electron transfer. Therefore, we only expect case I, III, VI, VII in Figure 7 to show RS due to MP-induced IPC at the largest current. This expectation is consistent with the cyclic voltammetry shown in Figure 9. At even higher current and voltage, the droplet may cover the whole electrode in case II, IV, V and lead to RS, too.

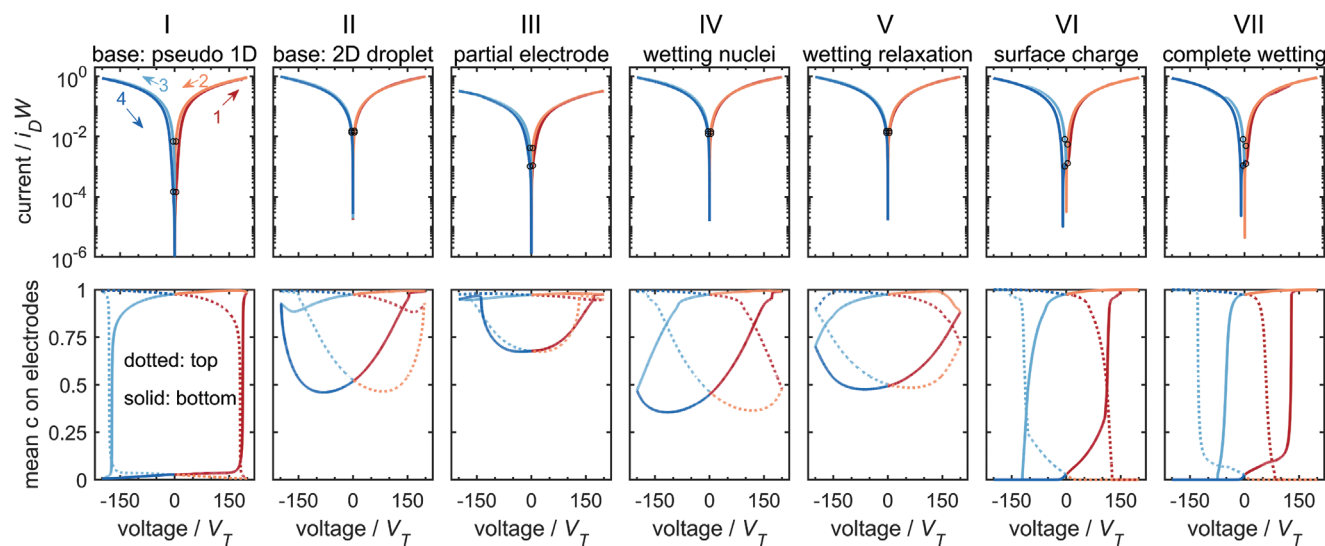
Since the ion-rich system needs much larger current and voltage for MP-induced RS, we expect that the ion-poor system is more useful for MP-based memories made from LTO-like materials.

## 6. Discussion and Conclusion

In this section, we first discuss the insights brought by this work on the understanding and optimization of MP-based memristors, then discuss possible extensions and improvements of the current model for general problems of coupled ion-electron transport, and finally make a conclusion.

### 6.1. Understanding and Optimization of MP-Based Memristors

To begin with, we want to point out the generalizability and limitations of the analysis of MP-based memristors in this work. The scaling analysis, including the scales for switching energy and time, should be general. However, our simulations are all based on LTO ( $\text{Li}_{4+3x}\text{Ti}_5\text{O}_{12}$ ) material, which goes through insulator-metal transition for  $x: 0 \rightarrow 1$ . We also assume that the surface resistance decreases with ion concentration, too. Therefore, the ion-poor system has lower electronic conductivity than the ion-rich system. Nevertheless, materials like  $\text{Li}_x\text{CoO}_2$  with  $x \in [0.5, 1]$  can show metal-insulator transition for increasing ion concentration, so the ion-rich system can have lower electronic conductivity. In addition, different



**Figure 9.** Current ( $\tilde{i} = I/i_D W$ , top row) and mean concentration on electrodes (bottom row) along with the applied voltage ( $\tilde{V} = V/V_T$ , where  $V_T = 0.025 V$ ) during cyclic voltammetry with voltage sweeping rate 50 (scaled by  $V_T/\tau_D$ ), for the ion-rich systems shown in Figure 7. The circles on the current–voltage curves mark the points with  $|\dot{V}| = 4$ , which guide the eyes to read the resistance ratio. The dimensional scales (values for a 50-nm-thick LTO film) are:  $\tau_D = L^2/D_p^0$  (25 s),  $i_D = D_p^0 F c_0/L$  ( $0.44 \mu A \mu m^{-2}$ ). The corresponding time evolution of concentration contour maps can be found in Movie S6.

materials may have different concentration-dependence for ion diffusivity and Fermi energy. Therefore, some of our conclusions obtained from simulations are only constrained to the LTO-like materials.

First, we want to see some general conclusions regardless of the specific ion-intercalation materials. From scaling analysis, we know that the switching time is mainly limited by ion diffusion time,  $\tau_D = L^2/D_p^0$ , and can be reduced by one or two orders of magnitude by increasing the electric currents or including surface charge and heterogeneity (Figure 5, Figure 8). The switching energy per device area has scale  $e_0 = i_D V_T \tau_D = \frac{D_p^0 L F c_0 V_T}{D_p^0}$ , which can also be reduced by manipulating surface conditions (Figure 5 and Figure 8). Generally, we prefer materials with smaller electronic conductivity and larger ionic conductivity for MP, to reduce the switching time and energy simultaneously. As a comparison, Li-ion battery electrodes usually require the ion-intercalation material to have both large electronic conductivity and large ion diffusivity.<sup>[1]</sup> In addition, we can make the device thinner to reduce the switching time and energy, and scale down the device to reduce energy cost.

We list values of  $\tau_D$  and  $e_0$  for 10-nm thick multiphase ion-intercalation nanofilms for different materials in Table 1. Note that here the “metallic” and “insulating” phases are usually judged from electronic bands, and the metallic phase may also have conductivity much smaller than traditional metals due to small electron mobility (e.g., LTO and MoS<sub>2</sub>). Though MP can occur in all those materials, LFP may not be used for MP-based memristors because it does not have significant resistance transition by changing ion concentration. Then, we use Figure 10 to show the estimation of the switching time and energy density of MP for all the materials listed in Table 1. Here, we estimate the switching time as  $\tau_D/10$  and energy density as  $e_0/10$ , to include all the possible reduction enabled by adjusting

boundary conditions and mean concentration. Among LTO, LCO, MoS<sub>2</sub>, and graphite, graphite should show the smallest switching time in the scale of 1  $\mu s$ , and MoS<sub>2</sub> should show the smallest switching energy in the scale of fJ for a 100 nm  $\times$  100 nm  $\times$  10 nm device. There is still a lot of room to find better materials for MP-based memristors.

In the introduction, we have compared the principles for the MP mechanism and other nonvolatile RS mechanisms, as shown in Figure 1. We then want to compare the performance of these mechanisms. First, we note that the MP mechanism for a single crystal with homogeneous electrodes only has two resistance states. Therefore, multiple states for MP-based memristors should be obtained from polycrystalline structures or heterogeneous electrodes. This is similar to the FT mechanism. As a comparison, the RBT and PC memories can have numerous states by controlling the bulk ion concentration and conductive filament length, respectively. In addition, we note that the switching time for both MP and RBT are both limited by ion diffusion but can be improved by electric currents. Though ns-pulse can be used to switch the states of RBT, the reading can take longer time to wait for the stabilization of the system. Since ion diffusion in solids is usually slow, MP and RBT may have smaller switching time compared with PC or FT. However, they should require smaller energy, especially compared with PC. Ion-modulated phase change should cost less energy than crystallization or amorphization. Finally, FT should have smaller switching time and energy than MP since local dipole rotation should be faster than ion migration. However, here we only consider the performances of switching energy and time, while other performances, material price and manufacturing process can make the comparison of the mechanisms more complex.

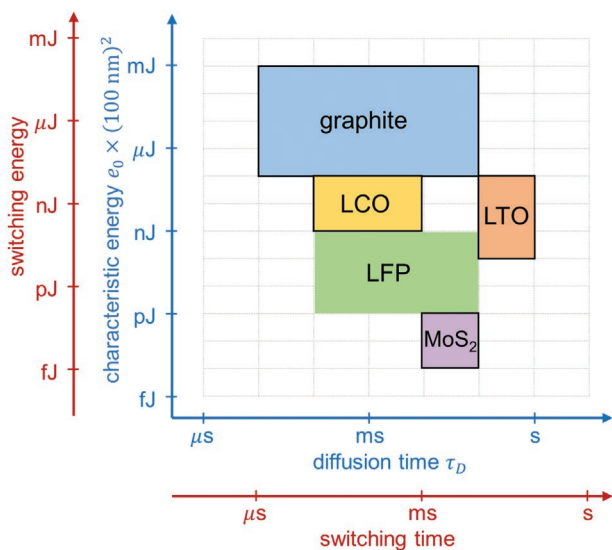
Next, we want to compare this work with our previous 1D model<sup>[26]</sup> in terms of the analysis of LTO memristors. The old 1D model, with neutral wetting and no surface charge or



**Table 1.** Scales of diffusion time  $\tau_D$  and characteristic energy density  $e_0 = i_D V_T \tau_D$  (where  $V_T$  is thermal voltage and  $i_D$  is electron diffusion current) for different ion-intercalation materials with ion diffusivity  $D_p$ , electronic conductivity  $\sigma_n$ , and thickness  $L = 10$  nm. In the first column, “i” represents the less conductive (insulating) phase, “m” represents the more conductive (metallic) phase. Among the materials in this table, only LTO, LCO, MoS<sub>2</sub>, and graphite can be used to make MP-based memristors. For the model in this work,  $\tau_D = L^2/D_p^0$  and  $i_D = D_p^0 c_0 F/L$  are well defined. For other cases, we estimate  $\tau_D = L^2/D_p$ , and  $i_D \approx \sigma_n^* V_T/L$  where  $\sigma_n^*$  is  $\sigma_n$  for a more-conductive component  $x$ .

Material	Ion diffusivity [ $\text{m}^2 \text{s}^{-1}$ ]	Electronic conductivity [ $\text{S cm}^{-1}$ ]	$\tau_D$ [s]	$e_0$ [ $\mu\text{J } \mu\text{m}^{-2}$ ]
Li <sub>4+3x</sub> Ti <sub>5</sub> O <sub>12</sub> (LTO)	$10^{-16}$ [this work, $D_p^0$ ]	$x = 1: 0.0035$ [this work]	1	0.055
$x: 0-1, i-m$	$10^{-16}-10^{-15}$ [7,79]	$x = 0: 10^{-13}-10^{-6}$ [78] $x = 1: 10^{-2}-1$ [7,78]	$10^{-1}-1$	$10^{-2}-10^1$
Li <sub>x</sub> CoO <sub>2</sub> (LCO)	$10^{-14}-10^{-12}$ [80]	$x = 0.5: 10^{2}$ [81] $x = 1: 10^{-4}-10^{-3}$ [81]	$10^{-4}-10^{-2}$	$10^{-1}-10^1$
$x: 0.5-1, m-i$				
Li <sub>x</sub> MoS <sub>2</sub> (MoS <sub>2</sub> )	$10^{-15}-10^{-14}$ [82]	$x = 0: 10^{-7}$ [83,84] $x = 1: 10^{-5}-10^{-4}$ [84,85]	$10^{-2}-10^{-1}$	$10^{-6}-10^{-4}$
$x: 0-1, i-m$				
Li <sub>x</sub> FePO <sub>4</sub> (LFP)	$10^{-15}-10^{-12}$ [80,86]	$x = 0.9: 10^{-2}$ [87]	$10^{-4}-10^{-1}$	$10^{-4}-10^{-1}$
$x: 0-1, i-i$		$x = 0, 1: 10^{-11}-10^{-10}$ [88]		
Li <sub>x</sub> C <sub>6</sub> (graphite)	$10^{-15}-10^{-11}$ [1]	$x = 0: 10^4$ [89]	$10^{-5}-10^{-1}$	$10^1-10^5$
$x: 0-1$ (4 stages), $m-m$		$x = 0.25: 10^5$ [89]		

surface energy relaxation, has already made a reasonable explanation of the LTO memristor experiments.<sup>[5]</sup> It shows that the ion-poor system switches faster and requires smaller current, which is qualitatively consistent with experiments. However, it overestimates the switching current by 2 to 3 orders of magnitude if we take material parameters from literature. In this work, the 2D phase pictures further show that the ion-rich system can require even larger current to squeeze the less-conductive ion-poor phase to fully cover the electrodes, in order to make significant resistance change. In addition, we show that surface charge, surface heterogeneity, and non-neutral wetting can reduce the switching current by over one order of magnitude (Figure 5b and Figure 8b).



**Figure 10.** The estimation of the switching time and energy for multiphase polarization (MP), for several multiphase Li<sup>+</sup>-intercalation materials shown in Table 1. Among these materials, LTO, LCO, MoS<sub>2</sub>, and graphite can be used to make MP-based memristors.

Finally, there is still no direct experimental observation of MP. In the future, we will seek for collaborators to do in-situ TEM<sup>[90,91]</sup> to show MP directly.

## 6.2. Improvements and Extensions of the Model

The current model can be improved in several aspects. First, we model the surface charge by a linear capacitor with only electronic charge considered. This greatly simplifies the problem. In the future, the model can be enriched by including the non-linear profiles of both ions and electrons in the space charge, and the dependence of capacitance on concentration and overpotential.<sup>[92–94]</sup> Second, we use an empirical Butler–Volmer equation with series resistance to describe the electron transfer kinetics at the electrode surface. This can also be improved by considering the physical mechanisms for electron transfer, such as tunneling and Schottky barrier.<sup>[57,95]</sup> Finally, the model can also be improved by including temperature change and mechanical effects.

The current model can also be extended for other materials and applications. For example, the model can also be extended to multi-stage phase-separating ion-intercalation materials, like graphite.<sup>[89]</sup> and WO<sub>3</sub>.<sup>[45]</sup> This should lead to multiple states switchable by MP without including bulk or surface heterogeneity. Besides, we can also modify the boundary conditions in order to analyze multiphase coupled ion-electron transport in other ion-intercalation memories like RBT. We also hope this work will inspire material scientists to explore the potential role of MP in other applications such as battery.

## 6.3. Conclusion

To summarize, in this work, we derive a phase-field model for a mixed ion-electron conductor sandwiched by ion-blocking electrodes, for which model we have included a comprehensive

boundary condition to consider the surface effects of electron transfer kinetics, non-neutral wetting, surface energy relaxation, and surface charge. Then we apply the model to the ion-intercalation material, and study the phenomenon of multiphase polarization (MP) driven by high electric currents and the resulting resistive switching (RS). We show that the surface heterogeneity, surface charge, and non-neutral wetting can reduce the switching current significantly, and show that the manipulation of a small amount of the more-conductive phase in less-conductive phase can be better for LTO-like materials. We also compare the physics and performance of MP with other non-volatile RS mechanisms, and show that MP-based memories require multiphase ion-intercalation materials with high ionic diffusivity, low electronic conductivity, and significant resistance change with concentration. The phenomenon of MP is a great example of the coupling of ion and electron transport, and the model can be extended in the future for other problems with similar physics.

## Supporting Information

Supporting Information is available from the Wiley Online Library or from the author.

## Acknowledgements

This work was supported by a grant from Ericsson. The authors would like to thank Danniel Cogswell, Michael Li, and Huada Lian for helpful discussions.

## Conflict of Interest

The authors declare no conflict of interest.

## Data Availability Statement

Data sharing is not applicable as the article describes entirely theoretical research.

## Keywords

coupled ion-electron transport, ion intercalation, phase-field modeling, resistive switching memories

Received: November 22, 2022

Revised: February 3, 2023

Published online:

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# ADVANCED FUNCTIONAL MATERIALS

## Supporting Information

for *Adv. Funct. Mater.*, DOI: 10.1002/adfm.202213621

Multiphase Polarization in Ion-Intercalation Nanofilms:  
General Theory Including Various Surface Effects and  
Memory Applications

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# Supplemental Material: Multiphase polarization in ion-intercalation nanofilms: general theory including various surface effects and memory applications

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(Dated: February 23, 2023)

## A. DERIVATION OF EQUATION 10

In the following, we will use integration by parts:

$$\int_{\Omega} \nabla a \cdot \mathbf{b} dV = \int_{\Omega} a \mathbf{n} \cdot \mathbf{b} dS - \int_{\Omega} a \nabla \cdot \mathbf{b} dV \quad (\text{S1})$$

where  $a$  is any scalar and  $\mathbf{b}$  is a vector.

We first derive  $\frac{\partial \mathcal{G}_1}{\partial t}$  :

$$\begin{aligned} \frac{\partial \mathcal{G}_1}{\partial t} &= \sum_{k=p,n} \int_{\Omega} \left( \frac{\partial g_k}{\partial c_k} \frac{\partial c_k}{\partial t} + \frac{\partial g_k}{\partial \nabla c_k} \cdot \frac{\partial \nabla c_k}{\partial t} \right) dV \\ &\quad + \int_{\Omega} \left( \sum_{k=p,n,d} \frac{\partial g_k}{\partial \phi} \right) \frac{\partial \phi}{\partial t} dV \\ &\quad + \int_{\partial \Omega} \mu_n \mathbf{J}_n \cdot \mathbf{n} dS \\ &= \sum_{k=p,n} \int_{\Omega} \left( \frac{\partial g_k}{\partial c_k} - \nabla \cdot \frac{\partial g_k}{\partial \nabla c_k} \right) \frac{\partial c_k}{\partial t} dV \\ &\quad + \int_{\partial \Omega} \frac{\partial g_k}{\partial \nabla c_k} \cdot \mathbf{n} \frac{\partial c_k}{\partial t} dS \\ &\quad + \int_{\Omega} \left( \sum_{k=p,n,d} z_k c_k F \right) \frac{\partial \phi}{\partial t} dV \\ &\quad + \int_{\partial \Omega} \mu_n \mathbf{J}_n \cdot \mathbf{n} dS \end{aligned} \quad (\text{S2})$$

Then we recognize that in the first integration,  $\frac{\partial g_k}{\partial c_k} - \nabla \cdot \frac{\partial g_k}{\partial \nabla c_k} = \mu_k$ , and  $\frac{\partial c_k}{\partial t} = -\nabla \cdot \mathbf{J}_k$ . Therefore,

$$\begin{aligned} &\int_{\Omega} \left( \frac{\partial g_k}{\partial c_k} - \nabla \cdot \frac{\partial g_k}{\partial \nabla c_k} \right) \frac{\partial c_k}{\partial t} dV \\ &= - \int_{\Omega} \mu_k \nabla \cdot \mathbf{J}_k dV \\ &= - \int_{\partial \Omega} \mu_k \mathbf{J}_k \cdot \mathbf{n} dS + \int_{\Omega} \nabla \mu_k \cdot \mathbf{J}_k dV \end{aligned} \quad (\text{S3})$$

Then we substitute this equation into Equation S2, and apply  $\partial g_k / \partial \nabla c_k = \kappa_k \nabla c_k$  and  $\mathbf{J}_p \cdot \mathbf{n} = 0$  on  $\partial \Omega$ , we can get Equation 10.

## B. DISCUSSION ON SURFACE ENERGY

In this part, we first discuss on the signs of surface energy that we expect without mathematical model, based on physical insights and literature. And then we see if these expectations are consistent with our model.

To begin with, we compare the free energy of an electric double layer (EDL, two parallel layer of opposite charges) and a capacitor. The free energy of the natural formation of an EDL, spontaneously formed at the interface between two materials without any externally applied voltage, should be negative [1]. This can be explained as below. The charge carriers in the two materials can have different chemical potential (Fermi energy at zero electric potential for electrons), so they tend to go from the high-energy side to the low-energy side, which will form the surface charges and develop an electric potential drop to balance the chemical energy drop. The above process occurs spontaneously, so the sign of the free energy should be negative. Although the electric double layer is often modeled as a capacitor, we should be careful about the differences and connections of those two. A capacitor can store energy so its own energy should be positive. However, the capacitor cannot be charged without external forces. A battery is needed to charge the capacitor. In another word, the free energy for an isolated circuit composed of a battery (an ideal voltage

source in series with a resistor) in series with a capacitor should be negative. If we assume constant capacitance for the EDL, then the formula for the free energy of an isolated EDL is the same as that of an isolated battery-capacitor circuit.

Then let us see if our model is consistent with the above analysis. Equation 16 (in combination with Equation 15) leads to

$$\gamma_s = \gamma_s^* + \frac{1}{2}C\eta^2 - \frac{1}{2}C(\Delta\phi)_0^2. \quad (\text{S4})$$

Therefore,  $\eta = 0$  leads to a negative EDL energy, while  $\Delta\phi_0 = 0$  leads to a positive capacitor energy. These are all consistent with our expectations. Then we can also check the second approach in Equation 18. We can change the limits of the integration, to get free energy for the formation of a natural EDL:

$$\gamma_s^0 - \gamma_s^* = \int_0^{C(\Delta\phi)_0} \Delta\mu_n \frac{d\Gamma}{z_n F} = -\frac{1}{2}C(\Delta\phi)_0^2, \quad (\text{S5})$$

which is as expected. This integral was actually used in Ref.[1] to derive the free energy of an EDL. We can also see that Equation 18 is the energy stored in one capacitor due to external applied voltage. Finally, the energy into and out of the interface has been considered in Equation 4, and can change the effective surface energy, which has been shown in Equation 19.

## C. SUPPLEMENTING FIGURES

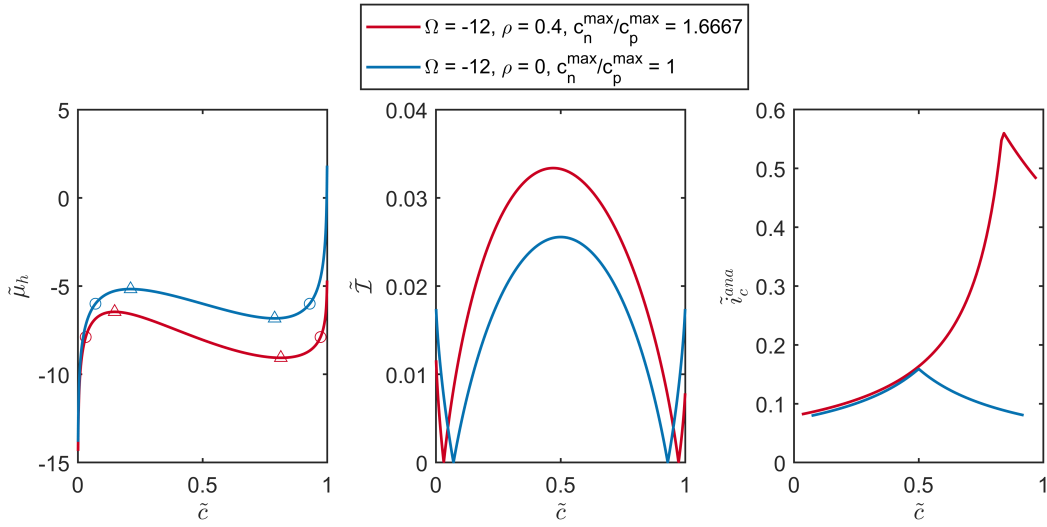


FIG. S1. The functions of  $\tilde{\mu}_h(\tilde{c})$ ,  $\tilde{I}(\tilde{c})$ , and  $\tilde{i}_c^{ana}(\tilde{c})$  for the regular solution model with two sets of typical parameters. In the left column, the circles label the binodal points and the triangles label the spinodal points.

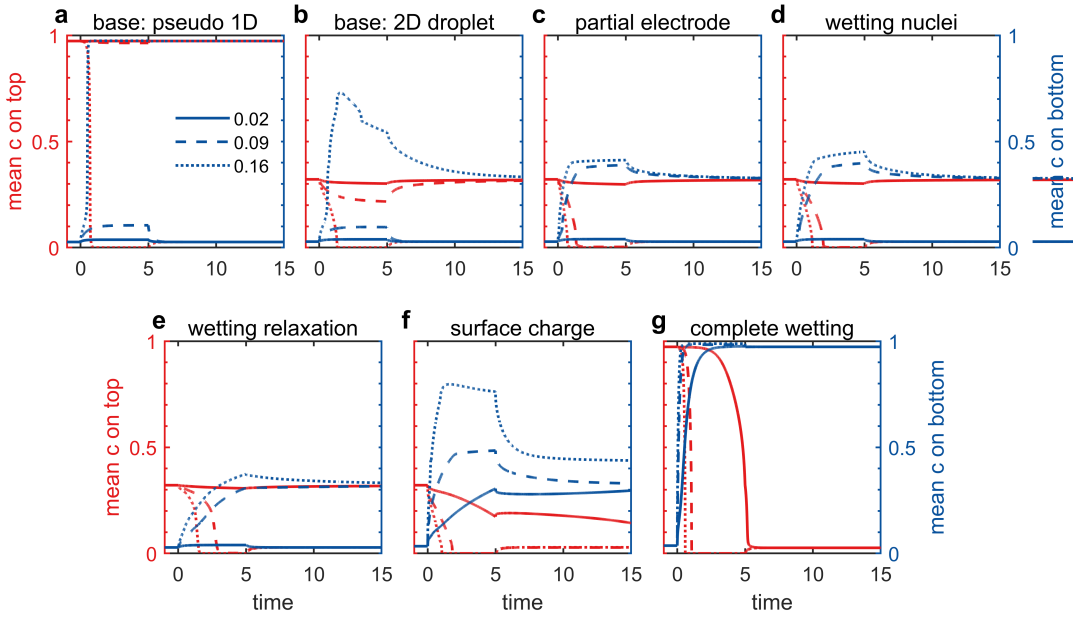


FIG. S2. Time evolution of the mean concentration on electrodes in the ion-poor systems, for all the cases shown in Figure 4. Parts of the relaxation periods before and after the applied current are also plotted here.

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[1] E. J. W. Verwey and J. T. G. Overbeek, *Theory of the stability of lyophobic colloids* (Elsevier, Amsterdam, 1948).



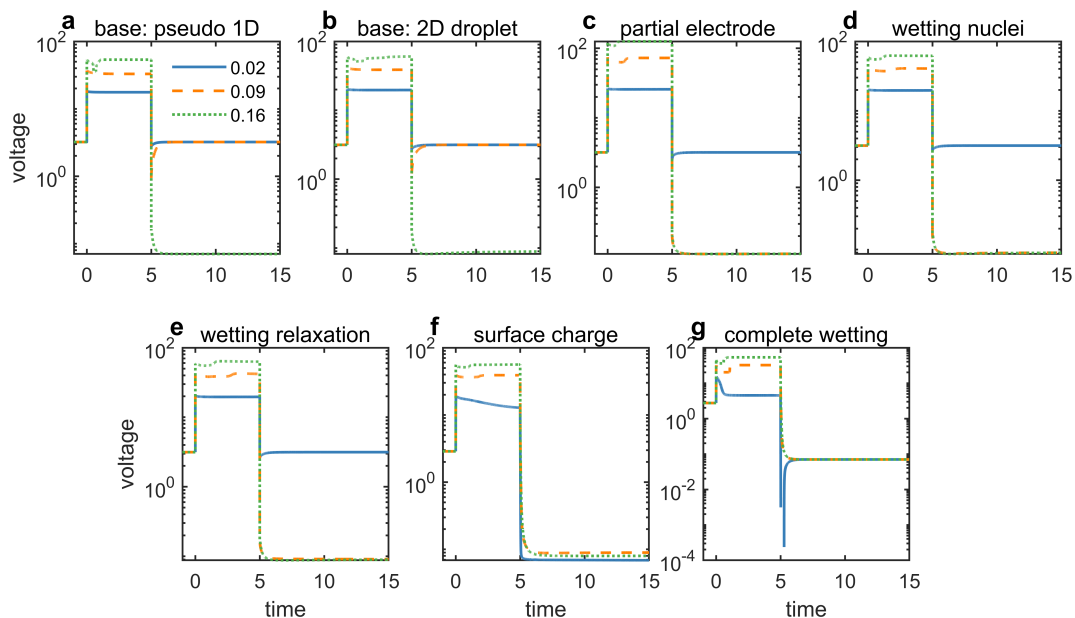


FIG. S3. Time evolution of the voltage applied to the ion-poor systems during the current step tests, for all the cases shown in Figure 4. Parts of the relaxation periods before and after the applied current are also plotted here.

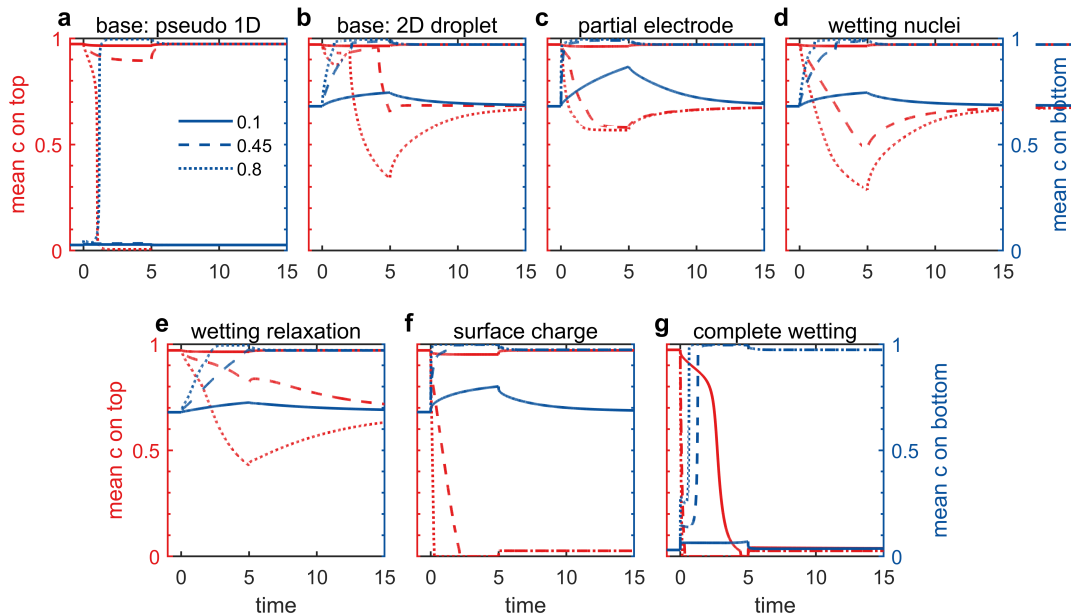


FIG. S4. Time evolution of the mean concentration on electrodes in the ion-rich system, for all the cases shown in Figure 7. Parts of the relaxation periods before and after the applied current are also plotted here.

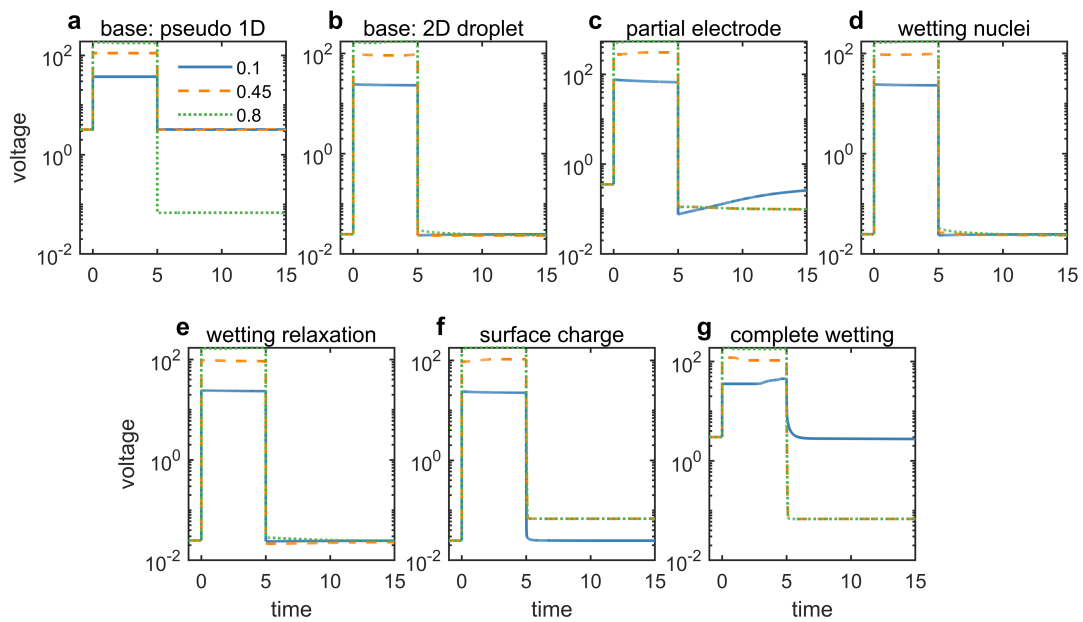


FIG. S5. Time evolution of the voltage applied to the ion-rich systems during the current step tests, for all the cases shown in Figure 7. Parts of the relaxation periods before and after the applied current are also plotted here.